An American National Standard

Standard Practice for Steel Castings, Welding, Qualifications of Procedures and Personnel¹

This standard is issued under the fixed designation A 488/A 488M; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

This standard has been approved for use by agencies of the Department of Defense.

1. Scope

- 1.1 This practice establishes the qualification of procedures, welders, and operators for the fabrication and repair of steel castings by electric arc welding.
- 1.1.1 Qualifications of a procedure and either or both the operator or welder under Section IX of the ASME Boiler and Pressure Vessel Code shall automatically qualify the procedure and either or both the operator or welder under this practice. P-number designations in the ASME grouping of base metals for qualification may be different than the category numbers listed in Table 1. Refer to Appendix X1 for a comparison of ASTM category numbers with the corresponding ASME P-Number designations.
- 1.2 Each manufacturer or contractor is responsible for the welding done by his organization and shall conduct the tests required to qualify his welding procedures, welders, and operators.
- 1.3 Each manufacturer or contractor shall maintain a record of welding procedure qualification tests (Fig. 1), welder or operator performance qualification tests (Fig. 2), and welding procedure specification (Fig. 3), which shall be made available to the purchaser's representative on request.
- 1.4 The values stated in either inch-pound units or SI units are to be regarded separately as standard. Within the text, the SI units are shown in brackets. The values stated in each system are not exact equivalents; therefore, each system must be used independently of the other. Combining values from the two systems may result in nonconformance with this practice.
- 1.5 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

2. Referenced Documents

2.1 ASTM Standards:

A 27/A 27M Specification for Steel Castings, Carbon, for

General Application²

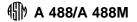
- A 148/A 148M Specification for Steel Castings, High Strength, for Structural Purposes²
- A 216/A 216M Specification for Steel Castings, Carbon, Suitable for Fusion Welding, for High-Temperature Service²
- A 217/A 217M Specification for Steel Castings, Martensitic Stainless and Alloy, for Pressure-Containing Parts, Suitable for High-Temperature Service²
- A 351/A 351M Specification for Castings, Austenitic, Austenitic–Ferritic (Duplex), for Pressure–Containing Parts²
- A 352/A 352M Specification for Steel Castings, Ferritic and Martensitic, for Pressure-Containing Parts, Suitable for Low-Temperature Service²
- A 356/A 356M Specification for Steel Castings, Carbon, Low Alloy, and Stainless Steel, Heavy-Walled for Steam Turbines²
- A 370 Test Methods and Definitions for Mechanical Testing of Steel Products³
- A 389/A 389M Specification for Steel Castings, Alloy, Specially Heat-Treated, for Pressure-Containing Parts, Suitable for High-Temperature Service²
- A 447/A 447M Specification for Steel Castings, Chromium-Nickel-Iron Alloy (25-12 Class), for High-Temperature Service²
- A 487/A 487M Specification for Steel Castings Suitable for Pressure Service²
- A 494/A 494M Specification for Castings, Nickel and Nickel Alloy²
- A 732/A 732M Specification for Castings, Investment, Carbon and Low Alloy Steel for General Application, and Cobalt Alloy for High Strength at Elevated Temperatures²
- A 743/A 743M Specification for Castings, Iron-Chromium, Iron-Chromium-Nickel, Corrosion-Resistant, for General Application²
- A 744/A 744M Specification for Castings, Iron-Chromium-Nickel, Corrosion-Resistant, for Severe Service²
- A 747/A 747M Specification for Steel Castings, Stainless, Precipitation Hardening²

¹ This practice is under the jurisdiction of ASTM Committee A01 on Steel, Stainless Steel and Related Alloys and is the direct responsibility of Subcommittee A01.18 on Castings.

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 $^{^{2}}$ Annual Book of ASTM Standards, Vol 01.02.

³ Annual Book of ASTM Standards, Vol 01.03.



RECOMMENDED FORM FOR MANUFACTURER'S RECORD OF WELDING PROCEDURE QUALIFICATION TESTS

| Procedure No | Date: | Welding Process: | | | | |
|--|----------------|---|-------------------|--|------------------------------|--------------------------------|
| | | of category No | | | | |
| | | ness Range Qualified | | | | |
| | | _ Weld Deposit A-Group N | | | | |
| Flux Designation: | Gas | Composition: | | No weath on the state of the st | , | |
| | | g Strip, if any: | | | | |
| | | Single or Multiple F | | | | |
| | | er Wire Diameter: | | | | |
| Trade Name: | Type of E | Backing: | | | | |
| Forehand or Backhand | : | _Amps: Volts | S | Inches/min: | | |
| Postheat Temperature | | Time at Temperature | | | | |
| | | | | | | |
| | | TENS | SION TEST RE | | | |
| Specimen No. | Width | Dimensions Thickness | Area | Ultimate Total Load, lb | Ultimate Unit Stress, psi | Nature of Failure and Location |
| | | | | | | |
| | | | BEND TEST I | | | |
| Specimen No |). | Results | | Specimen No. | | Results |
| Who by virtue of thes Test Conducted By: per We certify that the st | se tests mee | Clock No Stants the welder performand Test No this record are correct a | ce qualification | ı. | | |
| with the requirements Signed: | | tandard | | | | |
| - 3 | | | facturer or Co | ntractor | | |
| Date: | | FIG | 6. 1 Report For | m 1 | | |
| | Recommend | ED FORM FOR MANUFACTURE | r's or Contrac | CTOR'S RECORD OF WEL | DER OR OPERATOR | |
| | | Perform | ANCE QUALIFICAT | TION TESTS | | |
| | | D | | | | |
| Clock No W | elding Process | S: | | | | |
| Position: | | | | | | |
| In accordance with Proc | | | to antogon, No | | | |
| Plate Thickness: | Range of | of category No Thickness Qualified: | _ to category inc | J | | • |
| Filler Metal Specification | No. | Group No F | | | | |
| Filler Metal A-Group No. | | . Group No. F Filler Metal Diameter | | | | |
| | Flux Desigr | nation or Gas Analysis: | | | | |
| | | GUIDED | BEND TEST | RESULTS | | |
| Specimen No |). | Results | | Specimen No. | | Results |
| | | | | | | |
| • | | _ Laboratory Test No | | | | |
| | | s record are correct and th | at the test welc | ds were prepared, weld | ded, and tested in a | accordance with ASTM |
| Signed: | | B.4 | faatuwar O- | atronto. | | |
| Date: | | Manu | facturer or Cor | itractor | | |
| | | | | | | |

FIG. 2 Report Form 2

A 757/A 757M Specification for Steel Castings, Ferritic and Martensitic, for Pressure-Containing and Other Appli-

cations, for Low-Temperature Service²
A 872/A 872M Specification for Centrifugally Cast



REPORT FORM 3

RECOMMENDED FORM FOR WELDING PROCEDURE SPECIFICATION

| 1. Title | 7. Preheat | | | | |
|--|--|--|--|--|--|
| Welding of A steel castings. A Indicate general material description, such as carbon, Cr-Mo, 12 Cr, etc. | 7.1 Preheat and interpass temperature shall be maintained in the range from to during | | | | |
| 2. Specification NoRev | A Indicate minimum temperature. Indicate maximum temperature. Indicate if preheat maintenance is during welding or until postweld near treatment is performed. | | | | |
| 3. Scope | 7.2 Preheat for tack welding of backing plates is the same as required for welding. | | | | |
| 3.1 Procedure Specification No covers the welding of A steel castings using the B welding process. | 7.3 Minimum temperature before applying heat shall be | | | | |
| A Indicate general material description as in Title. B Indicate specific welding process, such as shielded metal arc, gas metal arc, etc. | 7.4 Local preheating to the temperatures indicated may be performed so that the heated area completely surrounds the weld preparation for a minimum distance of ^A in any direction. | | | | |
| 4. Base Material | A Indicate minimum distance for local preheating. | | | | |
| 4.1 The base material shall conform to the specifications for ^A | 8. Welding Position | | | | |
| which is found in materials category number ⁸ | 8.1 Welds shall be made in the ^A position. | | | | |
| A Insert here reference to ASTM designation or indicate chemical analysis and physical properties. | A Indicate position or positions in which the welding will be performed. See Fig. 4. | | | | |
| # Indicate category number from Table 1. | 9. Electrical Characteristics | | | | |
| 4.2 Base material shall be in the ^A heat treated condition before welding. | 9.1 The current used shall beA. The base material | | | | |
| A Indicate heat treatment before welding. | A Indicate whether direct or alternating current. If direct, state whether non- | | | | |
| 5. Filler Metal | pulsed or pulsed. If pulsed, state frequency. B Indicate whether electrode positive (EP) or electrode negative (EN) output | | | | |
| 5.1 The filler metal shall conform to ANSI/AWS Specification which is found in weld metal analysis group A | terminal of power supply is used. | | | | |
| ^Indicate appropriate American Welding Society specification number and filler metal classification (e.g., A5.1 E7018). **Indicate A Number from Table 4. | Wire Diameter ^A Amperage ^A Range ^A Voltage ^A | | | | |
| 5.2 Flux for submerged arc welding shall conform to the following nominal composition: | | | | | |
| **Indicate chemical composition or trade designation. 5.3 Shielding gas for gas shielded arc welding shall conform to the following nominal composition: **A | A Indicate for each diameter of electrode, the amperage, the range of amperage permitted, and the voltage requirements. For welding processes using wire, indicate wire diameter, wire feed speed, and current requirements. | | | | |
| A Indicate the single gas or proportional parts of mixed gases and flow rates. | 9.3 Electrodes subject to moisture absorption must be stored and handled to maintain dryness according to the following: | | | | |
| 6. Preparation of Base Material | A Where applicable, indicate electrode care instructions. | | | | |
| 6.1 Metal removal shall be performed by ^A A Indicate method of metal removal, such as chipping, grinding, carbon arc cutting, flame cutting etc. Also indicate whether preheat is required during metal | 10. Welding Details10.1 The width of any pass of welding shall not exceed^A | | | | |
| removal. | times the size of the filler metal used. | | | | |
| 6.2 Configuration of the weld preparation for partial penetration welds shall conform to the following geometry: A | A Indicate the number for controlling the maximum width. 10.2 Craters shall be properly filled before each interruption of the | | | | |
| A Indicate minimum root radius and minimum side wall angle. 6.3 Configuration of the weld preparation for full penetration welds shall conform to the following geometry: | arc. 10.3 Slag or flux shall be removed on any bead before depositing the next successive bead. | | | | |
| A Indicate minimum side wall angle. | 10.4 Interpass inspection shall be performed according to the | | | | |
| 6.4 Backing plates shall be used for welding full penetration welds. Backing plates shall be made from steel and shall fit the back of | following: A A Indicate degree of interpass inspection required. | | | | |
| the cavity with a minimum gap of ⁸ A Indicate material of backing plate. | 10.5 Peening shall be performed according to the following: A A Indicate the degree of peening required. Indicate any limits on peening first | | | | |
| ^a Indicate dimension of maximum gap. 6.5 Surfaces of the weld preparation shall be cleaned of all oil, | and last layers. 11. Post-Weld Heat Treatment | | | | |
| grease, dirt, scale, slag, shot blasting grit, or any foreign material which may be harmful to the quality of the weld. Surfaces of backing plates | 11.1 Post-weld heat treatment shall consist of the following: ^A | | | | |
| when used shall also meet the same cleanliness requirements. 6.6 All surfaces of the weld preparation shall be inspected as | A Indicate the heating and cooling rates, holding temperatures and times. | | | | |
| follows: A | 12. Inspection | | | | |
| A Indicate type of inspection. | 12.1 Inspection of the completed weld shall be performed according to the following: A | | | | |

FIG. 3 Report Form 3

A Indicate degree of inspection.



Ferritic/Austenitic Stainless Steel Pipe for Corrosive Environments⁴

A 890/A 890M Specification for Castings, Iron-Chromium-Nickel-Molybdenum Corrosion-Resistant, Duplex (Austenitic/Ferritic) for General Application²

A 990/A 990M Specification for Castings, Iron-Nickel-Chromium and Nickel Alloys, Specially Controlled for Pressure Retaining Parts for Corrosive Service²

A 995/A 995M Specification for Castings, Austenitic-

Ferritic (Duplex) Stainless Steel, for Pressure-Containing Parts²

2.2 American Society of Mechanical Engineers:

ASME Boiler and Pressure Vessel Code, Section IX⁵ 2.3 *American Welding Society:*

ANSI/AWS 3.0 Definitions for Welding and Cutting⁶

TABLE 1 Categories of Base Materials

| Category Number | Material Description | ASTM Specification | Grades |
|--------------------|--|------------------------------|--|
| 1 | Carbon steel (carbon less than 0.35 %, tensile strength less than or equal to 70 ksi [480 MPa]). | A 27/A 27M | all grades |
| | , | A 216/A 216M | WCA, WCB |
| | | A 352/A 352M | LCB, LCA |
| | | A 356/A 356M | 1 |
| | | A 732/A 732M | 1A, 2A |
| | | A 757/A 757M | A1Q |
| 2 | Carbon steel (tensile strength greater than 70 ksi [480 MPa]). Carbon-manganese steel (tensile strength equal to or greater than 70 ksi but less than 90 ksi [620 MPa]). | A 148/A 148M | 80-40 |
| | | A 216/A 216M | WCC |
| | | A 352/A 352M | LCC |
| | | A 732/A 732M | 2Q, 3A |
| | | A 757/A 757M | A2Q |
| 3 | Carbon and carbon-manganese steel (tensile strength equal to or greater than 90 ksi [620 MPa]). | A 732/A 732M | 3Q, 4A, 4Q, 5N |
| 4 | Low-alloy steel (annealed, normalized, or normalized and tempered. Tensile strength less than 85 ksi [585 MPa]). | A 148/A 148M | 80-50 |
| | Toriono otrorigar loco triar co noi [coo viii a]). | A 217/A 217M | WC1, WC4, WC5, WC6, WC9 |
| | | A 352/A 352M | LC1, LC2, LC3, LC4 |
| | | A 356/A 356M | 2, 5, 6, 8 |
| | | A 389/A 389M | C23, C24 |
| | | A 487/A 487M | 11A, 12A, 16A |
| | | A 757/A 757M | B2N, B3N, B4N |
| 5 | Low-alloy steel (annealed, normalized, or normalized and tempered. | A 148/A 148M | 90-60, 105-85 |
| Ü | Tensile strength equal to or greater than 85 ksi [585 MPa]). | A 217/A 217M | C5, C12, C12A, WC11 |
| | Toriono on origin oqual to or groater than oo her too mir ajj. | A 356/A 356M | 9, 10, C12 |
| | | A 487/A 487M | 1A, 1C, 2A, 2C, 4A, 4C, 6A, 8A, 9A, 9C, 10A, 13A |
| | | A 732/A 732M | 6N. 15A |
| | | A 757/A 757M | D1N1, D1N2, D1N3, E2N1, E2N2, E2N3 |
| 6 | Low-alloy steel (quenched and tempered) | A 148/A 148M | 00 60 405 95 445 05 420 445 425 425 450 425 |
| b | Low-alloy steer (quenched and tempered) | A 140/A 140W | 90-60, 105-85, 115-95, 130-115, 135-125, 150-135, 160-145, 165-150, 165-150L, 210-180, 210-180L, 260-210, 260-210L |
| | | A 352/A 352M | LC2-1, LC1, LC2, LC3, LC4, LC9 |
| | | A 487/A 487M | 1B, 1C, 2B, 2C, 4B, 4C, 4D, 4E, 6B, 7A, 8B, 8C, |
| | | A 401/A 401W | 9A, 9B, 9C, 9D, 9E, 10B, 11B, 12B, 13B, 14A |
| | | A 732/A 732M | 7Q, 8Q, 9Q, 10Q, 11Q, 12Q, 13Q, 14Q |
| | | A 752/A 752M A 757/A 757M | B2Q, B3Q, B4Q, C1Q, D1Q1, D1Q2, D1Q3, E1Q, |
| | | A TOTAL TOTAL | E2Q1, E2Q2, E2Q3 |
| 7 | Ferritic stainless steel | A 743/A 743M | CB-30, CC-50 |
| 8 | Martensitic stainless steel | A 217/A 217M | CA-15 |
| U | martonomo otaninego oteen | A 352/A 352M | CA6NM |
| | | A 356/A 356M | CA6NM |
| | | A 487/A 487M | CA15-A, CA15-B, CA15-C, CA15-D, CA15M-A, CA6NM-A, CA6NM-B |
| | | A 743/A 743M | CA-15, CA-15M, CA6NM, CA-40, CA6N, CB6 |
| | | A 757/A 757M | E3N |

⁴ Annual Book of ASTM Standards, Vol 01.01.

⁵ Available from the American Society of Mechanical Engineers, 345 E. 47th St., New York, NY 10017.

 $^{^{6}}$ Available from the American Welding Society, 550 NW LeJeune Rd., P.O. Box 351040, Miami, FL 33135.

TABLE 1 Continued

| Category Number | Material Description | ASTM Specification | Grades |
|--------------------|---|--------------------|---|
| 9 | Low-carbon austenitic stainless steel (carbon equal to or less than 0.03 %) | A 351/A 351M | CF-3, CF-3A, CF-3M, CF-3MA, CF-3MN, CK-3MCUN, CG3M, CN3MN |
| | | A 743/A 743M | CF-3, CF-3M, CF-3MN, CK-3MCUN, CN-3M, CG3M, CN3MN |
| | | A 744/A 744M | CF-3, CF-3M, CK-3MCUN, CG3M, CN3MN |
| 10 | Unstabilized austenitic stainless steel (carbon greater than 0.03 %) | A 351/A 351M | CE-8MN, CF-8, CF-8A, CF-8M, CF-10, CF-10M, CG-8M, CH-8, CH-10, CH-20, CG6MMN, CF10S1MNN, CE20N |
| | | A 447/A 447M | Type I |
| | | A 743/A 743M | CF-8, CG-12, CF-20, CF-8M, CF-16F, CF10SMNN, CH-20, CG-8M, CE-30, CG6MMN, CH10, CF16Fa |
| | | A 744/A 744M | CF-8, CF-8M, CG-8M |
| 11 | Stabilized austenitic stainless steel | A 351/A 351M | CF-8C, CF-10MC, CK-20, HK-30, HK-40, HT-30, CN-7M, CT-15C |
| | | A 447/A 447M | Type II |
| | | A 743/A 743M | CF-8C, CN-7M, CN-7MS, CK-20 |
| | | A 744/A 744M | CF-8C, CN-7M, CN-7MS |
| 12 | Duplex (austenitic-ferritic) stainless steel | A 351/A 351M | CD3MWCuN, CD-4MCU |
| | , | A 872/A 872M | J93183, J93550 |
| | | A 890/A 890M | 1A, 1B, 2A, 3A, 4A, 5A, 6A |
| | | A 995/A 995M | 1B, 2A, 3A, 4A, 5A, 6A |
| 13 | Precipitation-hardened austenitic stainless steel | A 747/A 747M | CB7CU-1, CB7CU-2 |
| 14 | Nickel-base alloys | A 494/A 494M | CW-12MW, CY-40 Class 1, CY-40 Class 2, CZ-100, M-35-1, M-35-2, M-30C, N-12MV, N-7M, CW-6M, CW-2M, CW-6MC, CX-2MW, CU5MCUC |
| | | A 990/A 990M | CW2M |

3. Terminology

3.1 *Definitions*— Definitions of terms relating to welding shall be in agreement with the definitions of the American Welding Society, ANSI/AWS A3.0.

4. Weld Orientation

- 4.1 *Orientation* The orientation of welds with respect to horizontal and vertical planes of reference are classified into four positions, namely, flat, horizontal, vertical, and overhead as shown in Fig. 4. Test material shall be oriented as shown in Fig. 4; however, an angular deviation of $\pm 15^{\circ}$ from the specified horizontal and vertical planes is permitted during welding.
- 4.2 Flat Position (Fig. 4(a))—This position covers plate in a horizontal plane with the weld metal deposited from above, or pipe or a cylindrical casting with its axis horizontal and rolled during welding so that the weld metal is deposited from above.
- 4.3 Horizontal Position (Fig. 4(b))—This position covers plate in a vertical plane with the axis of the weld horizontal, or pipe or a cylindrical casting with its axis vertical and the axis of the weld horizontal.
- 4.4 *Vertical Position* (Fig. 4(c))—In this position the plate is in a vertical plane with the axis of the weld vertical.
- 4.5 Overhead Position (Fig. 4(d))—In this position the plate is in a horizontal plane with the weld metal deposited from underneath.
- 4.6 Horizontal Fixed Position (Fig. 4(e))—In this position the pipe or cylindrical casting has its axis horizontal and the welding groove in a vertical plane. Welding shall be done

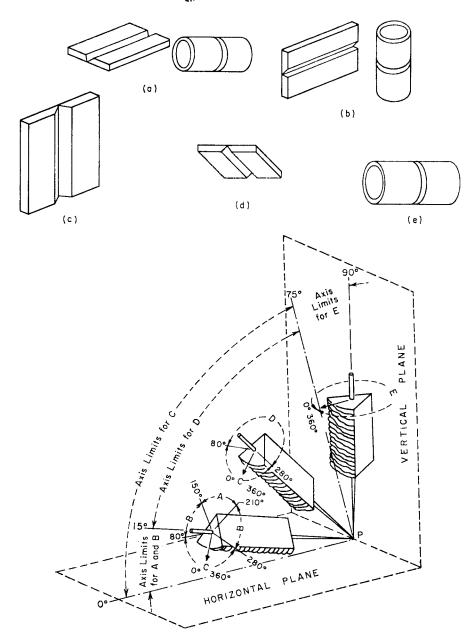
without rotating the pipe or casting so that the weld metal is deposited from the flat, vertical, and overhead position.

4.7 *Qualification*— Qualification in the horizontal, vertical, or overhead position shall qualify also for the flat position. Qualification in the horizontal fixed position, or in the horizontal and vertical and overhead positions, shall qualify for all positions (Fig. 4(*f*)).

5. Preparation of Test Plate

- 5.1 Procedure qualification testing shall be performed on cast or wrought material having the same category number as the casting being welded. Test material shall be subjected to the same heat-treatment before and after welding as will be applied to the casting. If the castings are not to be postweld heat-treated, then the test material is not to be postweld heat-treated. Test plate material for performance qualification testing is covered in 12.2.
- 5.2 The dimensions of the test plate shall be such as to provide the required number of test specimens.
- 5.3 The test joint shall be welded using the type of welding groove proposed in the welding procedure. The dimensions of the welding groove are not essential variables of the welding procedure.
- 5.4 The thickness of the test plate shall depend on the range of thickness to be qualified as shown in Table 2 and Table 3.
- 5.5 The joint preparation shown in Fig. 5 shall qualify the supplier for all welding on steel castings.
- 5.6 Where pipe or a cylindrical casting is used for qualification, it is recommended that a minimum nominal diameter of 5 in. [125 mm] and a minimum thickness of 3/8 in. [10 mm] be used.

∰ A 488/A 488M



Tabulation of Positions of Groove Welds

| Position | Diagram Reference | Inclination of Axis, ° | Rotation of Face,° |
|------------|----------------------|------------------------|-------------------------|
| Flat | A | 0 to 15 | 150 to 210 |
| Horizontal | В | 0 to 15 | 80 to 150 210 to 280 |
| Overhead | С | 0 to 75 | 0 to 80 280 to 360 |
| Vertical | D E | 15 to 75 75 to 90 | 80 to 280 0 to 360 |

Note 1—(a) Flat Position; (b) Horizontal Position; (c) Vertical Position; (d) Overhead Position; (e) Horizontal Fixed Position; (f) Positions of Groove Welds

FIG. 4 Orientation of Welds

TABLE 2 Type and Number of Test Specimens and Range of Thicknesses Qualified—(Procedure)

| Thickness, t, of Test Plate or Pipe as | Range of Thicknesses Qualified ^A | | Type and Number of Tests Required $^{\mathcal{B}}$ | | | |
|--|--|-----------------|--|-----------|-----------|-----------|
| Welded, in. [mm] | min, in. [mm] | max | Reduced Section Tension | Side Bend | Face Bend | Root Bend |
| 1/16 to 3/8 [1.6 to 9.5], incl | 1/16 [1.6] | 2t ^C | 2 | | 2 | 2 |
| Over 3/8 [9.5], under 3/4 [19.0] | 3/16 [4.8] | 2 <i>t</i> | 2 | | 2 | 2 |
| 3/4 [19.0] to under 11/2 [38.1] | 3/16 [4.8] | 2 <i>t</i> | 2 | 4 | | |
| 1½ [38.1] and over | 3/16 [4.8] | 8 [203] | 2 | 4 | | |

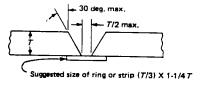
^A For repair welding, the minimum thickness requirements do not apply.

TABLE 3 Type and Number of Test Specimens and Thickness Limits Qualified—(Performance)

| Thickness, t, of Test Plate or Pipe as | Thickness Qualified | Type and Number of Tests Required ^A | | |
|---|---------------------|--|-----------|-----------|
| Welded, in. [mm] | Thickness Qualified | Side Bend | Face Bend | Root Bend |
| Up to % [9.5], incl | 2t | | 1 | 1 |
| Over % [9.5], under ¾ [19.0] ^B | 2 <i>t</i> | | 1 | 1 |
| Over % [9.5], under ¼ [19.0] ^B | 2 <i>t</i> | 2 | | |
| 3/4 [19.0], and over | max to be welded | 2 | | |

^A A total of four specimens are required to qualify for Position 1(e) of Fig. 4. Refer to Fig. 17 and Fig. 18.

^B Either the face- and root-bend tests or the side-bend tests may be used for thicknesses from % to ¾ in. [9.5 to 19.0 mm].



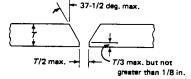


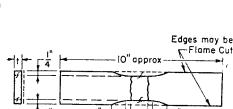
FIG. 5 Joint Preparation

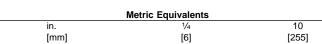
6. Types of Tests

- 6.1 Four types of tests are used in the qualification procedure as follows:
- 6.1.1 *Tension Test* Tests in direct tension are used in the procedure qualification to measure the strength of groove-weld joints.
- 6.1.2 *Bend Test*—Guided bend tests are used in the procedure and performance qualification tests to check the degree of soundness and ductility of groove-weld joints.
- 6.1.3 Charpy Impact Test—Charpy V-notch impact test specimens are used in the procedure qualification to determine the impact strength of weld metal deposited in groove-type joints.
- 6.1.4 *Radiographic Test*—Radiographic examination in accordance with 12.6 of a length of weld may be used to prove the ability of operators and welders to make sound welds.

7. Tension Test

- 7.1 *Specimens*—Tension tests shall conform to the requirements of 7.1.1 or 7.1.2.
- 7.1.1 All thicknesses of plate may be tested using reducedsection specimens conforming to the requirements of Fig. 6. All thicknesses of pipe or cylindrical castings having an outside diameter greater than 3 in. [75 mm] may be tested using reduced-section specimens conforming to the requirements of Fig. 7.
- 7.1.1.1 A single specimen of full-plate or full-pipe thickness shall be used for thicknesses up to and including 1 in. [25 mm].
 - 7.1.1.2 For plate or pipe thicknesses greater than 1 in. [25





This Section Machined

preferably by Milling

FIG. 6 Reduced-Section Tension Specimen for Plate

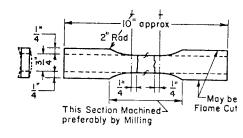
mm], single or multiple specimens may be used.

- 7.1.1.3 When multiple specimens are used, each set shall represent a single required tension test. Collectively, all of the specimens required to represent the full thickness of the weld at one location shall comprise a set.
- 7.1.1.4 When multiple specimens are necessary, the entire thickness shall be mechanically cut into a minimum number of approximately equal strips of a size that can be tested in the available equipment. Each specimen shall be tested and meet the requirements of 7.1.4.
- 7.1.2 Turned specimens conforming to the requirements of Fig. 8 may be used for tension tests.
- 7.1.2.1 For thicknesses up to and including 1 in. [25 mm], a single turned specimen may be used, which shall be a specimen of the largest diameter possible for the test coupon thickness.
 - 7.1.2.2 For thicknesses greater than 1 in. [25 mm], multiple

^B Either the face- and root-bend tests or the side-bend tests may be used for thicknesses from % to ¾ in. [9.5 to 19.0 mm].

^C The maximum thickness qualified with pipe smaller than 5 in. [127 mm] is two times the thickness of the pipe but not more than ¾ in. [19.0 mm].

∰ A 488/A 488M



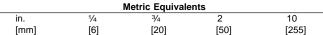
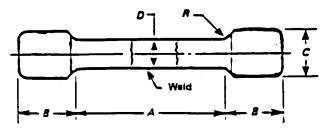


FIG. 7 Reduced-Section Tension Specimen for Pipe

Note 1—Reduced section A should not be less than width of weld plus 20.



| | Standard Dimensions, in. | | | | |
|-----------------------------|--------------------------|-----------------------|-----------------------|-----------------------|--|
| | (a) | (b) | (c) | (d) | |
| | 0.505 | 0.353 | 0.252 | 0.188 | |
| | Specimen ^A | Specimen ^B | Specimen ^C | Specimen ^D | |
| A—Length of reduced section | [Note] | [Note] | [Note] | [Note] | |
| D—Diameter | 0.500 ± 0.010 | 0.350 ± 0.007 | 0.250 ± 0.005 | 0.188 ± 0.003 | |
| R-Radius of fillet | 3/8, min | 1/4, min | 3/16, min | 1/8, min | |
| B—Length of end section | 13/8, approx. | 11/8, approx. | 7⁄8, approx. | ½, approx. | |
| C—Diameter of | 3/4 | 1/2 | 3/8 | 1/4 | |

^A Use maximum diameter specimen (a), (b), (c), or (d) that can be cut from the section.

FIG. 8 Alternate Reduced-Section Tension Specimen

specimens shall be cut through the full thickness of the weld with their centers parallel to the metal surface and not over 1 in. [25 mm] apart. The centers of the specimens adjacent to the metal surfaces shall not exceed 5/8 in. [16 mm] from the surface.

- 7.1.2.3 When multiple specimens are used, each set shall represent a single required tension test. Collectively, all of the specimens required to represent the full thickness of the weld at one location shall comprise a set. Each specimen shall be tested and meet the requirements of 7.1.4.
 - 7.1.3 The weld shall be in the center of the reduced section.
- 7.1.4 In order to meet the requirements of the tension test, specimens shall have a tensile strength not less than the specified tensile strength of the base material. If the specimen breaks in the base metal outside of the weld or fusion line, the test shall be accepted as meeting the requirements, provided

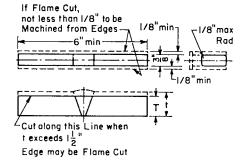
the strength is not more than 5 % below the specified minimum tensile strength of the base metal.

7.2 Tension Test— Tension tests shall be conducted in accordance with Test Methods and Definitions A 370.

8. Guided Bend Test

- 8.1 Specimens—Guided bend test specimens shall be prepared by cutting the test plate or pipe to form specimens of approximately rectangular cross section. The cut surfaces shall be designated the sides of the specimen. The other two surfaces shall be called the face and root surfaces, the face surface having the greater width of weld. Guided bend test specimens are of three types depending on which surface (side, face, or root) is on the convex (outer) side of the bent specimen. (Fig. 9 and Fig. 10.)
- 8.1.1 *Side Bend*—The weld is transverse to the longitudinal axis of the specimen which is bent so that one of the side surfaces becomes the convex surface of the bent specimen.
- 8.1.2 Face Bend—The weld is transverse to the longitudinal axis of the specimen which is bent so that the face surface becomes the convex side of the bent specimen.
- 8.1.3 *Root Bend*—The weld is transverse to the longitudinal axis of the specimen which is bent so that the root surface becomes the convex side of the bent specimen.
- 8.2 Guided Bend Tests—Table 2 and Table 3 give the number and type of guided bend specimens that are to be used in the procedure and performance qualification tests.
- 8.2.1 Specimens of base metal thicknesses over 1.5 in. [38 mm] may be cut into approximately equal strips between ³/₄ in. [19 mm] and 1.5 in. [38 mm] wide for testing, or the specimens may be bent at full width. If multiple specimens are used, one complete set shall be made for each required test. Each specimen shall be tested and meet the requirements of 8.2.3.
- 8.2.2 Guided bend specimens shall be bent in jigs that are in substantial accordance with Fig. 11, Fig. 12, and Fig. 13. The side of the specimen turned toward the gap of the jig shall be the face for face-bend specimens, the root for root-bend specimens, and the side with the greater number of defects, if any, for side-bend specimens. The specimen shall be forced into the die by applying load on the plunger until the curvature

Note 1—For plates over $1\frac{1}{2}$ in. [38.1 mm] thick, cut specimen into approximately equal strips between $\frac{3}{4}$ in. [20 mm] and $\frac{1}{2}$ in. [40 mm] wide and test each strip.



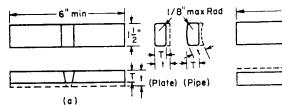
| Metric Equivalents | | | | | |
|---------------------------|-----|------|------|-------|--|
| in. | 1/8 | 3/8 | 11/2 | 6 | |
| [mm] | [3] | [10] | [40] | [155] | |
| FIG. 9 Side-Bend Specimen | | | | | |

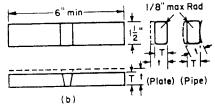
^B Weld should be in center of reduced section.

^C Where only a single coupon is required the center of the specimen should be midway between the surfaces.

^D The ends may be threaded or shaped to fit the holders of the testing machine in such a way that the load is applied axially.

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Metric Equivalents

| in. | 1/8 | 11/2 | 6 | | |
|--|--|------|-------|--|--|
| [mm] | [3] | [40] | [155] | | |
| (a) Transverse Face-Bend Specimen—Plate and Pipe | | | | | |
| | t, in. [mm] T, in. [mm] (all Ferrous Materials | | | | |

| 1/16 to 1/8 [1.6 to 3.2] |
|--------------------------|
| 1/8 to 3/8 [3.2 to 9.5] |
| > % [9.5] |

| t | |
|-------|----|
| t | |
| 3/6[0 | 51 |

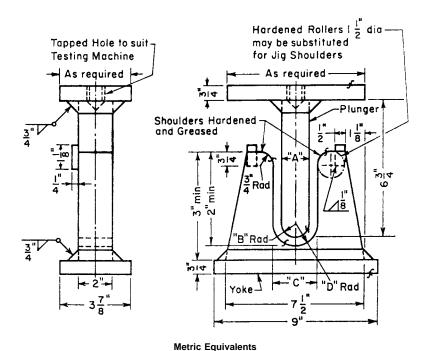
Metric Equivalents

| in. 1½ 6 [mm] [3] [40] [155] |
|---------------------------------|
|---------------------------------|

(b) Transverse Root-Bend Specimen—Plate and Pipe

Note-Weld reinforcement and backing strip or backing ring, if any, shall be removed flush with the surface of the specimen. If a recessed ring is used, this surface of the specimen may be machined to a depth not exceeding the depth of the recess to remove the ring, except that in such cases the thickness of the finished specimen shall be that specified above.

FIG. 10 Transverse Face- and Root-Bend Specimens, for Pipe and Plate



| in. | 1/8 | 1/4 | 1/2 | 3/4 | 11/8 | 11/2 | 2 | 3 | 37/8 | 63/4 | 71/2 | 9 |
|------|-----|-----|------|------|------|------|------|------|-------|-------|-------|-------|
| [mm] | [3] | [5] | [15] | [20] | [30] | [40] | [50] | [75] | [100] | [170] | [190] | [230] |
| | | | | | | | | | | | | |

| Specimen Thickness, in. [mm] | <i>A</i> , in. [mm] | <i>B</i> , in. [mm] | <i>C</i> , in. [mm] | <i>D</i> , in. [mm] |
|------------------------------------|------------------------|---------------------|------------------------|------------------------|
| ³⁄8 [9.5] | 1½ [38.1] | 3/4 [19.0] | 2% [60.3] | 13/16 [30.2] |
| t | 4 <i>t</i> | 2 <i>t</i> | 6t + 1/8 | 3 <i>t</i> + ½16 |
| | | | [3.2] | [1.6] |

FIG. 11 Guided-Bend Test Jig

of the specimen is such that a ½-in. [3.2-mm] diameter wire cannot be inserted between the die and the specimen, or so that the specimen is bottom ejected if the alternate roller type jig is used. When using the wrap-around jig (Fig. 13), the side of the specimen turned toward the roller shall be the face for face-bend specimens, the root for root-bend specimens, and the side with the greater defects, if any, for side-bend specimens. When specimens wider than 1.5 in. [38.1 mm] are to be bent,

the test jig mandrel must be at least 0.25 in. [6.4 mm] wider than the specimen width.

8.2.3 In order to meet the requirements of this test, the guided bend specimens shall have no cracks or other open defects exceeding 1/8 in. [3.2 mm] measured in any direction on the convex surface of the specimen after bending. However, cracks occurring on the corners of the specimen during testing shall not be considered unless there is definite evidence that

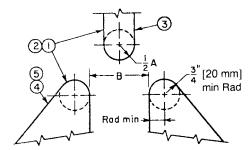


FIG. 12 Alternative Roller-Equipped Guided-Bend Test Jig

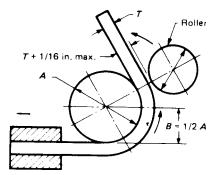


FIG. 13 Guided Bend Wrap-Around Jig

they result from slag inclusions or other internal defects.

8.2.4 Where the ductility of the parent metal is such as to render it incapable of meeting the bend test requirements of 8.2.2 and 8.2.3, the bend test shall be conducted in the following manner: A bend bar comprised of parent metal heat treated to the ductility and strength requirements of the applicable specification shall be bent to failure. The side-bend specimen shall then be capable of being bent to within 5° of the angle thus determined.

9. Charpy Impact Test

9.1 Application— Charpy V-notch impact tests of the weld metal and heat-affected zone shall be made when such tests are

required for the parent metal by the material specification, or specified by the purchaser, and shall apply to the qualification of the welding procedure for fabrication and repair. When postweld heat treatment consists of a full reheat treatment of the welded part, thus eliminating the HAZ, impact testing of the HAZ shall not be required.

9.2 Test Methods— Test methods for Charpy V-notch impact tests shall be in accordance with Test Methods and Definitions A 370 and conducted at the same temperature as required for the parent metal.

9.2.1 Test Specimens— Each set of three weld metal impact specimens shall be taken across the weld with the notch in the weld metal. Each specimen shall be oriented so that the notch is normal to the surface of the material and one face of the specimen shall be within $\frac{1}{16}$ in. [1.6 mm] of the surface of the metal. Heat-affected zone coupons for impact specimens shall be taken transverse to the weld and etched to define the heat-affected zone. The notch shall be cut normal to the material surface in the heat-affected zone to include as much heat-affected zone as possible in the resulting fracture (Fig. 14(a)). Where the material thickness permits, the axis of a heat-affected zone specimen may be inclined to allow the root of the notch to align parallel to the fusion line (Fig. 14(b)).

9.2.2 Acceptance Criteria—Acceptance criteria for the weld metal and heat-affected zone shall be the same as that required by the material specification for the parent metal.

10. Procedure Qualification

10.1 Each manufacturer or contractor shall record in detail the welding procedure used in qualifying under this practice. A suggested form (Fig. 1) is included with this practice.

10.2 The number of tests required to qualify a procedure for various thickness ranges shall be as shown in Table 2.

10.3 Test specimens shall be removed from the plate or pipe or cylindrical casting as shown in Fig. 15, Fig. 16, Fig. 17, and Fig. 18.

10.4 In order to qualify, test specimens shall meet the

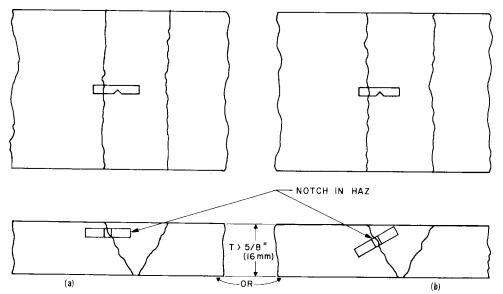
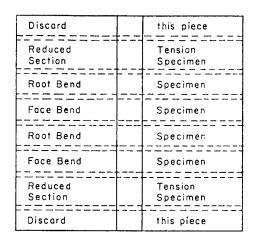


FIG. 14 Location of Notch in Charpy Specimens Shall Be In HAZ Midway Between Center and Surface



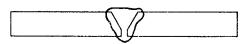


FIG. 15 Order of Removal of Test Specimens from Test Plate 1/16 to 3/4 in. [1.6 to 19.0 mm] Thick

| Discard | this piece |
|--------------------|---------------------|
| Side Bend | Specimen |
| Reduced Section | Tension Specimen |
| Side Bend | Specimen |
| Side Bend | Specimen |
| Reduced Section | Tension Specimen |
| Side Bend | Specimen |
| Discard | this piece |



FIG. 16 Order of Removal of Test Specimens from Welded Test Plates over ¾ in. [19.0 mm] Thick (May be Used for Thicknesses ¾ to ¾ in. [9.5 to 19.0 mm])

requirements of 7.1.4, 8.2.3, or 8.2.4.

11. Requalification of a Procedure

- 11.1 A welding procedure must be set up as a new procedure and must be requalified when any of the changes in essential variables listed in 11.1.1 to 11.1.12, inclusive, are made. Changes other than those listed may be made without requalification, provided the procedure is revised to show these changes.
- 11.1.1 A change from a base material listed under one category number in Table 1 to a material listed under another category number. When two base materials having different category numbers are welded together, a procedure qualification must be performed for the combination.
 - 11.1.2 A change in the weld-deposit analysis or electrode

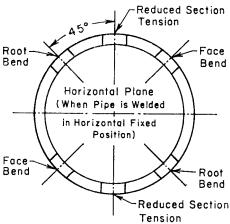


FIG. 17 Order of Removal of Test Specimens from Welded Pipe or Cylindrical Castings 1/16 to 3/4 in. [1.6 to 19.0 mm] Thick

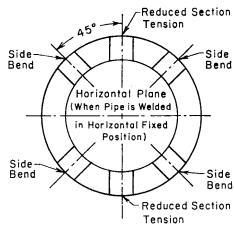


FIG. 18 Order of Removal of Test Specimens from Welded Pipe or Cylindrical Castings over ¾ in. [19.0 mm] Thick (May be Used for Thicknesses ¾ to ¼ in. [9.5 to 19.0 mm])

type will require requalification under any of the following conditions:

- 11.1.2.1 A change from one A number in Table 4 to any other A number. Qualification with A No. 1 shall qualify for A No. 2 and vice versa. In lieu of an A number designation, the nominal chemical composition of the weld deposit shall be indicated on the Welding Material Specification (Fig. 3). Designation of nominal chemical composition may also be by reference to the AWS classification (where such exists), the manufacturer's trade designation, or other established procurement documents.
- 11.1.2.2 A change from one F number in Table 5 to any other F number.
- 11.1.3 A decrease of 100°F [55°C] or more in the minimum specified preheat temperature.
- 11.1.4 A significant change in the post heat-treating temperature or time cycle.
- 11.1.5 A change in the method of backing up, or its omission if previously used.
 - 11.1.6 A change in the welding process.
- 11.1.7 In submerged arc welding, where the alloy content of the weld metal is largely dependent upon the composition of the flux used, any change in any part of the welding procedure

TABLE 4 A Numbers—Classification of Weld Metal Analysis for Procedure Qualification

| A No. | Types of Wold Denseit | Analysis ^A | | | | | | |
|-------|-----------------------------------|-----------------------|----------------|--------------|----------------|--------------|-------|--|
| A NO. | Types of Weld Deposit | C, % | Cr, % | MO, % | Ni, % | Mn, % | Si, % | |
| 1 | Mild steel | 0.15 | | | | 1.60 | 1.00 | |
| 2 | Carbon-molybdenum | 0.15 | 0.50 | 0.40 to 0.65 | | 1.60 | 1.00 | |
| 3 | Chromium (0.4 to 2 %)—molybdenum | 0.15 | 0.40 to 2.00 | 0.40 to 0.65 | | 1.60 | 1.00 | |
| 4 | Chromium (2 to 6 %)—molybdenum | 0.15 | 2.00 to 6.00 | 0.40 to 1.50 | | 1.60 | 2.00 | |
| 5 | Chromium (6 to 10.5 %)—molybdenum | 0.15 | 6.00 to 10.50 | 0.40 to 1.50 | | 1.20 | 2.00 | |
| 6 | Chromium-martensitic | 0.15 | 11.00 to 15.00 | 0.70 | | 2.00 | 1.00 | |
| 7 | Chromium-ferritic | 0.15 | 11.00 to 30.00 | 1.00 | | 1.00 | 3.00 | |
| 8 | Chromium-nickel | 0.15 | 14.50 to 30.00 | 4.00 | 7.50 to 15.00 | 2.50 | 1.00 | |
| 9 | Chromium-nickel | 0.30 | 25.00 to 30.00 | 4.00 | 15.00 to 37.00 | 2.50 | 1.00 | |
| 10 | Nickel to 4 % | 0.15 | | 0.55 | 0.80 to 4.00 | 1.70 | 1.00 | |
| 11 | Manganese-molybdenum | 0.17 | | 0.25 to 0.75 | 0.85 | 1.25 to 2.25 | 1.00 | |
| 12 | Nickel-chromium-molybdenum | 0.15 | 1.50 | 0.25 to 0.80 | 1.25 to 2.80 | 0.75 to 2.25 | 1.00 | |

A Single values shown above are maximum.

that would result in the important alloying elements in the weld metal being outside of the specification range of chemistry given in the welding procedure specification.

- 11.1.8 In submerged arc welding a change in the nominal composition or type of flux used (requalification is not required for a change in flux particle size).
- 11.1.9 For submerged arc welding a change from a filler metal containing 1.75 to 2.25 % manganese to filler metal containing less than 1.00 % manganese or vice versa shall require requalification. The presence or absence of up to 0.5 % molybdenum in the filler metal analysis shall not require requalification.
- 11.1.10 For submerged arc welding a change in filler metal analysis in Table 4 from one A number to another.
- 11.1.11 In gas metal arc welding and gas tungsten arc welding.
- 11.1.11.1 A change from the qualified single gas to any other single gas or to a mixture of gases, or a change in specified percentage composition of gas mixture.
- 11.1.11.2 A decrease of 10 % or more in the rate of flow of shielding gas or mixture.
- 11.1.12 For gas metal arc welding a change in the consumable electrode from bare (solid) to flux cored, or vice versa.
- 11.1.13 Qualification of Category 10 base materials shall also qualify Category 9 base materials, and vice versa. Separate welding procedures are required for each category.

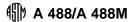
12. Performance Qualification of Welders or Operators

- 12.1 All welders and operators welding castings under this practice shall pass the welder qualification test. The welder or operator successfully performing the procedure qualification test is automatically qualified for performance.
- 12.1.1 Each welder or operator shall be qualified for each welding process (GTAW, GMAW, SMAW, FCAW, etc.) he uses. The welder or operator successfully qualified with one procedure for a process is qualified to weld with any other welding procedure using the same welding process, unless requalification is required by Section 13.
- 12.2 Test Plate—The test plate or pipe or cylindrical casting shall be the same as that used in the procedure qualification with respect to groove dimensions, filler metal, etc. Groove dimensions as shown in Fig. 5 may be used. The welding procedure shall conform to that given in the procedure quali-

- fication. For performance qualification, carbon steel plate, pipe, or cylindrical castings may be used for qualification of materials having a total alloy content of less than 6 %.
- 12.3 *Number of Tests* The number and type of tests to qualify a performance shall be as shown in Table 3.
- 12.4 Test specimens shall be removed from the plate or pipe or cylindrical casting as shown in Fig. 15, Fig. 16, Fig. 17, and Fig. 18.
- 12.5 The guided bend test shall meet the requirements as specified in 8.2.3.
- 12.6 Alternative to the mechanical tests required in 12.3, 12.4, and 12.5, the qualification test plate for welders and operators making groove welds using SMAW, GTAW, FCAW, or GMAW (except the short circuiting mode of transfer) processes may be examined by radiography using a technique shown by penetrameters to equal or exceed 2 % sensitivity. The weld to be radiographed shall be at least 6 in. [150 mm] long for welders and operators, or alternatively, a 3-ft [0.9-m] length of the first production weld made by a welding operator may be examined by radiography.
- 12.6.1 Final acceptance of the welds shall be based on the radiographic requirements of Section IX of the ASME Boiler and Pressure Vessel Code.
- 12.6.2 If a production weld is selected for welder or operator qualification and it does not meet the radiographic standards, the welder or operator has failed the test. In the event the production weld requires welder or operator qualification, the entire production weld made by that welder or operator shall be radiographed and repaired by a qualified welder or operator. Alternatively, the entire weld shall be removed and replaced by a qualified welder or operator.
- 12.7 Each manufacturer or contractor shall maintain a record of the procedures, including essential variables, under which the welders and operators are examined. A suggested form for recording such information is shown in Fig. 2.

13. Requalification of Welders and Operators

- 13.1 A welder must be requalified when one of the changes in essential variables listed in 13.2 and 13.3 is made in the procedure, or as provided in 13.4 or 13.5.
- 13.2 A change in the weld deposit metal to a weld deposit metal having a different F number, or to a weld deposit metal not covered under Table 4. Qualification under any F number



up to and including F4 shall qualify a welder for all lower F numbers.

- 13.3 A change in the method of backing up, or its omission if previously used.
- 13.4 When a welder has not used the specified process for three months or more.
- 13.5 When there is a reason to question his ability to make welds that meet this practice.
- 13.6 Requalification under 13.4 or 13.5 need only be made in a single thickness.

14. Retests

14.1 A welder or operator who fails to meet the require-

ments for one or more test specimens may be retested under the conditions described in 14.2 and 14.3.

- 14.2 When an immediate retest is made, the welder or operator shall make two test plates, each of which shall meet the requirements. If he fails these tests, he must undergo further training before a retest is permitted.
- 14.3 When a welder has had further training, a single retest is permitted.

15. Keywords

15.1 qualifications; steel castings; welding

TABLE 5 F Numbers—Grouping of Filler Metals for Qualification

| | | ANGUANG Clearification |
|----------|--|--|
| F No. | ANSI/AWS Specification | ANSI/AWS Classification |
| 1 | SFA-5.1 & 5.5 | EXX20, EXX22, EXX24, EXX27, EXX28 |
| 1 | SFA-5.4 | EXX25, EXX26 |
| 2 | SFA-5.1 & 5.5 | EXX12, EXX13, EXX14, EXX19 |
| 3 | SFA-5.1 & 5.5 | EXX10, EXX11 |
| 4 | SFA-5.1 & 5.5 | EXX15, EXX16, EXX18, EXX48 |
| 4 | SFA-5.4 (other than austenitic and duplex) | EXX15, EXX16, EXX17 |
| 5 | SFA-5.4 (austenitic and duplex) | EXX-15, EXX-16, EXX-17 |
| 6 | SFA-5.2 | RX |
| 6 | SFA-5.17 | FXX-EXX, FXX-ECX |
| 6 | SFA-5.9 | ERXX, ECXX, EQXX |
| 6 | SFA-5.18 | ERXXS-X, EXXC-X, EXXC-XX |
| 6 | SFA-5.20 | EXXT-X |
| 6 | SFA-5.22 | EXXXT-X |
| 6 | SFA-5.23 | FXX-EXXX-X, FXX-ECXXX-X, FXX-EXXX-XN, FXX-ECXXX-XN |
| 6 | SFA-5.25 | FESXX-EXXXXX-EW |
| 6 | SFA-5.26 | EGXXS-X, EGXXT-X |
| 6 | SFA-5.28 | ERXXS-X, EXXC-X |
| 6 | SFA-5.29 | EXXTX-X |
| 6 | SFA-5.30 | INXXXX |
| 41 | SFA-5.11 | ENi-1 |
| 41 | SFA-5.14 | ERNi-1 |
| 41 | SFA-5.30 | IN61 |
| 42 | SFA-5.11 | ENiCu-7 |
| 42 | SFA-5.14 | ERNiCu-7 |
| 42 | SFA-5.14 | ERNiCu-8 |
| 42 | SFA-5.30 | IN60 |
| 43 | SFA-5.11 | ENiCrFe-1 |
| 43 | SFA-5.11 | ENiCrFe-2 |
| 43 | SFA-5.11 | ENiCrFe-3 |
| 43 | SFA-5.11 | ENICrFe-4 |
| 43 | SFA-5.11 | ENICrFe-7 |
| 43 | SFA-5.11 | ENiCrFe-9 |
| 43 | SFA-5.11 | ENiCrFe-10 |
| 43 | SFA-5.11 | ENICrCoMo-1 |
| 43 | SFA-5.11 | ENiCrMo-2 |
| 43 | SFA-5.11 | ENICrMo-3 |
| 43 | SFA-5.11 | ENICIMO-5 |
| 43 | SFA-5.11 | ENICIMO-0 |
| 43 | SFA-5.11 | ERNiCr-3 |
| 43 | SFA-5.14 SFA-5.14 | ERNICI-3 ERNICI-4 |
| 43 | SFA-5.14 SFA-5.14 | ERNICI-4 ERNICI-6 |
| 43 | SFA-5.14 SFA-5.14 | ERNICI-0 ERNICIFE-5 |
| 43 43 | SFA-5.14 SFA-5.14 | ERNICIFE-5 ERNICIFE-6 |
| 43 | SFA-5.14 SFA-5.14 | ERNICIFE-0 ERNICIFE-7 |
| | | |
| 43 | SFA-5.14 | ERNICrFe-8 |
| 43 | SFA-5.14 | ERNICIFE-11 |
| 43 | SFA-5.14 | ERNICrCoMo-1 |
| 43 | SFA-5.14 | ERNICIMo-2 |
| 43 | SFA-5.14 | ERNiCrMo-3 |
| 43 | SFA-5.30 | IN82 |
| 43 | SFA-5.30 | IN62 |
| 43 | SFA-5.30 | IN62A |
| 44 | SFA-5.11 | ENIMo-1 |
| 44 | SFA-5.11 | ENIMo-3 |
| 44 | SFA-5.11 | ENiMo-7 |

TABLE 5 Continued

| F No. | ANSI/AV | NS Specification | ANSI/AWS Classification |
|-------|----------|------------------|-------------------------|
| 44 | SFA-5.11 | ENiMo-8 | |
| 44 | SFA-5.11 | ENiMo-9 | |
| 44 | SFA-5.11 | ENiMo-10 | |
| 44 | SFA-5.11 | ENiCrMo- | 4 |
| 44 | SFA-5.11 | ENiCrMo- | 5 |
| 44 | SFA-5.11 | ENiCrMo- | 7 |
| 44 | SFA-5.11 | ENiCrMo- | 10 |
| 44 | SFA-5.11 | ENiMo-13 | } |
| 44 | SFA-5.11 | ENiMo-14 | |
| 44 | SFA-5.14 | ERNiMo- | 1 |
| 44 | SFA-5.14 | ERNiMo- | 2, ERNiMo-3 |
| 44 | SFA-5.14 | ERNiMo- | 7 (Alloy B-2) |
| 44 | SFA-5.14 | ERNiMo- | 3 |
| 44 | SFA-5.14 | ERNiMo- | |
| 44 | SFA-5.14 | ERNiMo- | 10 |
| 44 | SFA-5.14 | ERNiCrM | 0-4 |
| 44 | SFA-5.14 | ERNiCrM | 0-5 |
| 44 | SFA-5.14 | ERNiCrM | o-7 (Alloy C-4) |
| 44 | SFA-5.14 | ERNiCrM | 0-10 |
| 44 | SFA-5.14 | ERNiCrM | 0-13 |
| 44 | SFA-5.14 | ERNiCrM | 0-14 |
| 44 | SFA-5.14 | ERNiCrW | Mo-1 |
| 45 | SFA-5.11 | ENiCrMo- | 1 |
| 45 | SFA-5.11 | ENiCrMo- | 9 |
| 45 | SFA-5.11 | ENiCrMo- | 11 |
| 45 | SFA-5.14 | ERNiCrM | 0-1 |
| 45 | SFA-5.14 | ERNiFeC | r-1 |
| 45 | SFA-5.14 | ERNiCrM | |
| 45 | SFA-5.14 | ERNiCrM | |
| 45 | SFA-5.14 | ERNiCrM | 0-11 |

APPENDIX

(Nonmandatory Information)

X1. PRACTICE A 488/A 488M CATEGORY NUMBER AND CORRESPONDING ASME P NUMBER

X1.1 Listed in Table X1.1 for information are the Practice A 488/A 488M categories of base metal casting specifications for welding qualifications and the corresponding P number

designations from Section IX of the ASME Boiler and Pressure Vessel Code:



TABLE X1.1 ASTM Categories of Base Metal Casting Specifications and Corresponding P Number Designations

Note 1—The P numbers are under the jurisdiction of the ASME Boiler and Pressure Vessel Code and may be subject to change subsequent to the effective date of this specification.

| | ASTM | | A 488/A 488M | ASME | | |
|---|--------|-------|--------------|-------|-----------|--|
| Specification | Grade | Class | Category No. | P No. | Group No. | |
| A 216/A 216M | WCA | | 1 | 1 | 1 | |
| ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | WCB | | 1 | 1 | 2 | |
| | WCC | | 2 | 1 | 2 | |
| | VVCC | | 2 | ' | 2 | |
| A 217/A 217M | WC1 | | 4 | 3 | 1 | |
| | WC4 | | 4 | 4 | 1 | |
| | WC5 | | 4 | 4 | 1 | |
| | WC6 | | 4 | 4 | 1 | |
| | WC9 | | 4 | 5A | 1 | |
| | C5 | | 5 | 5B | 1 | |
| | C12 | | | | | |
| | | | 5 | 5B | 1 | |
| | CA-15 | | 8 | 6 | 3 | |
| A 351/A 351M | CF3 | | 9 | 8 | 1 | |
| | CF3A | | 9 | 8 | 1 | |
| | CF8 | | 10 | 8 | 1 | |
| | CF8A | | 10 | 8 | 1 | |
| | | | | | | |
| | CF10 | | 10 | 8 | 1 | |
| | CF10M | | 10 | 8 | 1 | |
| | CF3M | | 9 | 8 | 1 | |
| | CF8M | | 10 | 8 | 1 | |
| | CF8C | | 11 | 8 | 1 | |
| | CH8 | | 10 | 8 | 2 | |
| | CH20 | | 10 | 8 | 2 | |
| | CK20 | | 11 | 8 | 2 | |
| | CN7M | | 11 | 45 | | |
| | CG6MMN | | 10 | 8 | 3 | |
| | CG8M | | 10 | 8 | 1 | |
| | CD4MCU | | 12 | 10H | 1 | |
| | CE8MN | | 10 | 10H | 1 | |
| | CT15C | | 11 | 45 | | |
| | | | | | | |
| A 352/A 352M | CA6NM | | 8 | 6 | 4 | |
| | LCA | | 1 | 1 | 1 | |
| | LCB | | 1 | 1 | 1 | |
| | LCC | | 2 | 1 | 2 | |
| | LC1 | | 4 | 3 | 1 | |
| | LC2 | | 4/6 | 9A | 1 | |
| | LC3 | | 4/6 | 9B | 1 | |
| | LC4 | | 4/6 | 9C | 1 | |
| | LC2-1 | | 4/6 | 11A | 5 | |
| | | | | | | |
| A 487/A 487M | 8 | Α | 5 | 5B | 1 | |
| | 8B | | 6 | 5C | 4 | |
| | 8C | | 6 | 5C | 4 | |
| | CA-15A | | 8 | 6 | 3 | |
| | CA-15B | | 8 | 6 | 3 | |
| | CA-15C | | 8 | 6 | 3 | |
| | CA-15D | | 8 | 6 | 3 | |
| | CA-15M | Α | 8 | 6 | 3 | |
| | CA 6NM | Α | 8 | 6 | | |
| | 1 | A | 5 | 10A | 1 | |
| | 1 | В | 6 | 10A | 1 | |
| | 2 | A | 5 | 10F | 1 | |
| | 2 | В | 6 | 10F | 1 | |
| | 4 | A | 5 | 10F | 1 | |
| | 4 | В | 6 | 11A | 3 | |
| | 16 | A | 4 | 1 | 2 | |
| | 16 | Δ | | | | |

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∰ A 488/A 488M

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