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Designation: E 1455 – 9703

# Standard Practice for Obtaining Colorimetric Data from a Visual Display Unit Using Tristimulus Colorimeters<sup>1</sup>

This standard is issued under the fixed designation E 1455; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

### INTRODUCTION

This practice provides directions for correcting the results obtained with tristimulus colorimeters when measuring the tristimulus values or chromaticity coordinates of colored displays. Tristimulus colorimeters approximate the CIE color matching functions  $\bar{x}$  ( $\lambda$ ),  $\bar{y}$  ( $\lambda$ ),  $\bar{z}$  ( $\lambda$ ) to make these measurements. The errors generated in measuring colors on a display may be minimized using this practice.

### 1. Scope

1.1 This practice is intended as an aid for improving the accuracy of colorimetric measurements made with tristimulus colorimeters on visual display units, such as cathode ray tubes (CRTs) and self-luminous flat-panel displays. It explains a useful step in the analysis of colorimetric data that takes advantage of the fact that light from such displays consists of an additive mixture of three primary colored lights. However, it is not a complete specification of how such measurements should be made.

1.2 This practice is limited to display devices and colorimetric instruments that meet linearity criteria as defined in the practice. It is not concerned with effects that might cause measurement bias such as temporal or geometric differences between the instrument being optimized and the instrument used for reference.

1.3 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

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<sup>&</sup>lt;sup>1</sup> This practice is under the jurisdiction of ASTM Committee E<sup>-12</sup> on <u>Color and</u> Appearance and is the direct responsibility of Subcommittee E12.06 on Appearance of Displays.

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# 2. Referenced Documents

# 2.1 ASTM Standards: <sup>2</sup>

E 284 Terminology of Appearance

E 1336 Test Method for Obtaining Colorimetric Data from a Video Display Unit by Spectroradiometry

E 1341 Practice for Obtaining Spectroradiometric Data from Radiant Sources for Colorimetry

2.2 ISO/CIE Standard:

CIE Standard Colorimetric Observers, ISO/CIE 10527: 1991 (E) (International Organization for Standardization, Geneva, 1991)<sup>3</sup>

# 3. Terminology

3.1 *Definitions:* Unless otherwise stated, definitions of appearance terms in Terminology E 284 are applicable to this practice. 3.2 *Definitions of Terms Specific to This Standard:* 

3.2.1 *calibration*, *n*— *in reference to a tristimulus colorimeter*, the process performed outside of this practice to adjust the tristimulus colorimeter to provide the best possible results for average or predefined conditions.

3.2.2 *optimization*, *n*— *in reference to a tristimulus colorimeter*, the process performed pursuant to this practice to adjust the tristimulus colorimeter or to interpret its readings to provide better results when applied to a particular display device.

3.2.3 *compatible*, *adj*— *in reference to a tristimulus colorimeter*, one so designed as to automate the procedure described in this practice.

# 4. Summary of Practice

4.1 Tristimulus colorimeters comprised of three or four detector channels are, in general, not amenable to accurate calibration that holds for all manner of usage with different illuminated devices and objects. This is because the spectral responsivities of their detector channels do not exactly match the defined Commission Internationale de L'Éclairage (CIE)  $\bar{x}(\lambda)$ ,  $\bar{y}(\lambda)$ ,  $\bar{z}(\lambda)$  functions. Factory or subsequent calibration reflects judgments and compromises that may not be readily apparent. Nevertheless, this practice provides guidance on how such a tristimulus colorimeter may be optimized for use with a particular video display device, providing better accuracy with that device than its more general calibration provides. An optimization matrix transforms the instrumental (measured) CIE *X*, *Y*, *Z* values into adjusted *X*, *Y*, *Z* values that are closer to the ideal. This matrix is determined by reference to a colorimeter with higher intrinsic accuracy. The method derives from the fact that the color stimulus functions from display devices are linear combinations of three primary functions and are not entirely arbitrary.

# 5. Significance and Use

5.1 This practice may be applied when tristimulus colorimeters are used to measure the colors produced on self-luminous video display devices such as CRTs and flat-panel displays, including electroluminescent (EL) panels, field emission displays (FEDs), and back-lit liquid crystal displays (LCDs). This practice is not meant to be a complete description of a procedure to measure the color coordinates of a display. Rather, it provides a method for obtaining more accurate results when certain conditions are met. It may be used by any person engaged in the measurement of color on display devices who has access to the requisite equipment.

5.2 This practice defines a class of tristimulus colorimeters that may be said to be compatible with this practice.

# 6. Background of Practice

# 6.1 Colorimetry:

6.1.1 Color measurement instruments consist, in general, of means to measure radiometric power as transmitted through a number of bandpass filters. Most commonly, electrical devices are used to measure the filtered light. They may be used with different filters in succession, or multiple devices may be used concurrently. In instruments called spectroradiometers, the radiometric power is measured through a large number (typically 30 to 500) of narrowband filters. (Practice E 1341 describes how a monochromator or polychromator (spectrograph) may be employed to filter and measure light in separate bands on the order of 1-nm wide.) In instruments called tristimulus colorimeters, the radiometric power is measured through three or four wideband filters. These filters may be constructed from dispersive elements (prisms and gratings) or from materials with selective spectral transmission or reflection. The latter may be either uniform or comprised of different patches, in a mosaic pattern, that provide the desired overall effect.

6.1.2 No matter how many filters are used, or in what manner, the goal of the measurement process is to determine tristimulus values *X*, *Y*, *Z*, as defined by ISO in its Standard 10527 and the CIE in its publication No. 15.2 (1).<sup>4</sup> For light with a color stimulus function  $\Phi(\lambda)$ ,

<sup>&</sup>lt;sup>2</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For Annual Book of ASTM Standards, Vol 06.01. volume information, refer to the standard's Document Summary page on the ASTM website.

<sup>&</sup>lt;sup>3</sup> Currently available through the U.S. National Committee of the CIE, c/o Mr. Thomas M. Lemons, TLA-Lighting Consultants, Inc., 7 Pond Street, Salem, MA 01970-4819. Also included in ASTM Standards on Color and Appearance, Fifth Edition, 1996.

<sup>&</sup>lt;sup>4</sup> BThe boldface numbers in parentheses refer to items in the list of R references at the end of this practice, standard.

$$X = k \int_{360 \text{ nm}}^{360 \text{ nm}} \Phi(\lambda) \bar{x}(\lambda) d\lambda \tag{1}$$

$$Z = k \int_{360 \text{ nm}}^{830 \text{ nm}} \Phi(\lambda) \bar{z}(\lambda) d\lambda \tag{1}$$

where:

*k* is 683 lm/W for emissive devices, such as displays, and  $\bar{x}$  ( $\lambda$ ),  $\bar{y}$  ( $\lambda$ ),  $\bar{z}$  ( $\lambda$ ) are color-matching functions. While the standard definition of *X*, *Y*, *Z* requires the use of the CIE 1931 2° color-matching functions, the mathematics described in this practice would also be applicable to any other set of color-matching functions, such as the CIE 1964 10° functions.

6.1.3 In practice, color measurement instruments compute X, Y, Z by the summation of the signals as measured through the various filters, each signal being multiplied by an appropriate calibration factor. In matrix notation:

$$\begin{bmatrix} X_{\rm m} \\ Y_{\rm m} \\ Z_{\rm m} \end{bmatrix} = \begin{bmatrix} C_{X1} C_{X2} C_{X3} \dots C_{Xf} \\ C_{Y1} C_{Y2} C_{Y3} \dots C_{Yf} \\ C_{Z1} C_{Z2} C_{Z3} \dots C_{Zf} \end{bmatrix} \begin{bmatrix} F_1 \\ F_2 \\ F_3 \\ \vdots \\ F_f \end{bmatrix}$$
(2)

where:

 $F_1$ ,  $F_2$ ,  $F_3$ , through  $F_f$  are the electrical signals from the *f* filtered detectors and the  $C_{ij}$  are calibration coefficients.  $X_m$ ,  $Y_m$ ,  $Z_m$  have subscripts to indicate that they are measured values rather than ideal ones.

6.1.4 In this practice, we presume that the color measuring instrument is linear: that each signal  $F_a$  is strictly proportional to the received optical power, that any zero-offset (background in darkness) is removed, that the proportionality for signal  $F_a$  is not affected by the value of signal  $F_b$ , and in the case of closely packed detectors (such as charge-coupled device (CCD) detector elements) no signal  $F_a$  spills over and affects signal  $F_b$  as it approaches saturation. These presumptions are amenable to experimental verification using methods beyond the scope of this practice (2).

6.1.5 The values of the matrix elements  $C_{ij}$  may be determined using criteria that depends on the design and intended application of the instrument. The full extent of this subject is beyond the scope of this practice. However, in general, for spectroradiometers  $(f \approx 30 \text{ to } 500)$ ,  $C_{Xj}$  reflects the tabulated value of  $\bar{x}(\lambda)$  near the center wavelength of Filter *j* as well as the spectral responsivity of the corresponding detector channel. (Likewise,  $C_{Yj}$  and  $C_{Zj}$  reflect  $\bar{y}(\lambda)$  and  $\bar{z}(\lambda)$ , respectively.) For tristimulus colorimeters, the choice of  $C_{ij}$  is discussed further, below. As a general matter, the instrument designer should choose passbands and matrix elements that balance accuracy, sensitivity, and other design requirements.

6.1.6 Tristimulus colorimeters are generally designed with filters that are intended to match the spectral responsivities of their detector channels to the CIE  $\bar{x}$  ( $\lambda$ ),  $\bar{y}$  ( $\lambda$ ),  $\bar{z}$  ( $\lambda$ ) functions. For such an instrument,

$$\begin{bmatrix} X_{m} \\ Y_{m} \\ Z_{m} \end{bmatrix} = \begin{bmatrix} C_{X1} 0 & 0 \\ 0 & C_{Y2} 0 \\ 0 & 0 & C_{Z3} \end{bmatrix} \begin{bmatrix} F_{1} \\ F_{2} \\ F_{3} \end{bmatrix}$$
(3)

where:

the non-zero  $C_{ij}$  matrix elements represent adjustable gains of the detector channels. However, the  $\bar{x}$  ( $\lambda$ ) function has two distinct lobes. This may be dealt with by splitting  $\bar{x}$  ( $\lambda$ ) into  $\bar{x}_{short}$  ( $\lambda$ ) and  $\bar{x}_{long}$  ( $\lambda$ ), each with a separate filter ( $F_1$  and  $F_2$ , respectively). For such an instrument,

$$\begin{bmatrix} X_{\rm m} \\ Y_{\rm m} \\ Z_{\rm m} \end{bmatrix} = \begin{bmatrix} C_{X1} C_{X2} 0 & 0 \\ 0 & 0 & C_{Y3} 0 \\ 0 & 0 & 0 & C_{Z4} \end{bmatrix} \begin{bmatrix} F_1 \\ F_2 \\ F_3 \\ F_4 \end{bmatrix}$$
(4)

Alternatively, the  $\bar{z}(\lambda)$  function may serve the role of  $\bar{x}_{short}(\lambda)$  since they have a similar shape,

$$\begin{bmatrix} X_{m} \\ Y_{m} \\ Z_{m} \end{bmatrix} = \begin{bmatrix} C_{X1} & 0 & C_{X3} \\ 0 & C_{Y2} & 0 \\ 0 & 0 & C_{Z3} \end{bmatrix} \begin{bmatrix} F_{1} \\ F_{2} \\ F_{3} \end{bmatrix}$$
(5)

In all of these cases, it is difficult to realize an exact match between the CIE color-matching functions and the actual spectral responsivities of the corresponding detector channels. This means that no choice of  $C_{ij}$  will provide perfect calibration for all applications of the instrument. The criteria for setting the  $C_{ij}$  might not be well documented for a particular instrument.

6.1.7 It is generally believed that spectroradiometers, with their many detector channels, may be calibrated to yield superior measurements of X, Y, Z for diverse applications. Nevertheless, the relative simplicity of tristimulus colorimeters and their commensurately lower cost have made them popular where the highest accuracy is not required.

6.2 Self-Luminous Displays:

6.2.1 A self-luminous display, such as a CRT, an electroluminescent (EL) panel, a field emission display (FED), or a back-lit liquid crystal display (LCD) generates colored light by the proportional superposition (addition) of primary colored lights  $\Phi_r$  ( $\lambda$ ),  $\Phi_g$  ( $\lambda$ ),  $\Phi_b$  ( $\lambda$ ). The subscripts represent red, green, and blue, the primary colors of an additive set. An arbitrarily colored patch on the visual display has one and only one color stimulus function  $\Phi(\lambda)$ ,

$$\Phi(\lambda) = a\Phi_r(\lambda) + b\Phi_g(\lambda) + c\Phi_b(\lambda)$$

(6)

where *a*, *b*, *c* are coefficients that are determined by the display electronics.

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6.2.2 The display electronics vary a, b, c over the face of the display in order to generate a colored image. For this practice, we presume that the display electronics may be set to make a, b, c uniform (perhaps after averaging nonobvious fine-structure) over a sufficient area of the display to permit measurements to be made on that area.

6.2.3 It is a requirement for the applicability of this practice that the display device behaves as stated in Eq 6. This practice does not represent that any particular display device will act as predicted by Eq 6, though those within the mentioned classes of devices might do so. The procedure for experimental verification of this property for a specific display device is beyond the scope of this practice (3).

### 6.3 Colorimetric Measurement of Displays:

6.3.1 Each of the primary color stimulus functions  $\Phi_r(\lambda)$ ,  $\Phi_g(\lambda)$ ,  $\Phi_b(\lambda)$  stimulates responses in the *f* detector channels that may be represented by a vector *F* (that is,  $F_r$ ,  $F_g$ ,  $F_b$ ). Given their construction, these vectors are linearly independent. (None of the three can be expressed as a linear combination of the other two.) While *F* is an element of an *f*-dimensional vector space, it is clear that only a three-dimensional subspace is spanned by the *F*'s of all possible color stimulus functions following Eq 6. Further, the mapping of *F* into  $(X_m, Y_m, Z_m)$  space by Eq 2 remains three dimensional. In other words, there is a one-to-one mapping of the vector (*a*, *b*, *c*) onto (*X*, *Y*, *Z*) by application of Eq 1; and, for a particular instrument with a fixed calibration matrix *C*, there is also a one-to-one mapping of the vector (*a*, *b*, *c*) onto (*X*\_m, *Y*\_m, *Z*\_m). From this we deduce that a matrix *R* exists that can be used to translate (*X*\_m, *Y*\_m, *Z*\_m) values into actual (*X*, *Y*, *Z*) values.

6.3.2 A colorimeter that takes advantage of this fact must provide means for implementing the matrix R. That is, all f filtered detector signals should contribute linearly toward the computation of each output,  $X_m$ ,  $Y_m$ ,  $Z_m$ , instead of using different detectors for each output. This idea was reported as long ago as 1973 by Wagner (4), and it has been expanded upon and rediscovered by others since then (5-910).

6.3.3 On the basis of this property, a tristimulus colorimeter can be optimized for use on a self-luminous display by the proper derivation of a matrix R for that display. We proceed on the assumptions that the components are sufficiently stable, and that similarly built displays have similar enough spectral primaries to make a derivation of R worthwhile. However, these assumptions should be quantified before accuracy claims are made in any specific situation.

6.3.4 On the basis of this property, a tristimulus colorimeter designed for use with displays need not produce signals F that are close to CIE tristimulus values. Signal/noise may be improved by matching the spectral responsivities of the filtered detectors to the emission spectra of the primary colors. In such designs, it is especially important to use a matrix R that is specific to the particular  $\Phi_r(\lambda)$ ,  $\Phi_g(\lambda)$ ,  $\Phi_b(\lambda)$ .

### 7. Optimization

#### 7.1 General:

7.1.1 Given the existence of a matrix R, how is it determined? Experimentally, the problem is one of comparing the data X, Y, Z from a reference colorimeter with the data  $X_m$ ,  $Y_m$ ,  $Z_m$  from the colorimeter being optimized, for a number of color samples at different display settings. From these data, R is calculated.

7.1.2 This practice is not directly concerned with the absolute accuracy of the measurements. It concerns the transfer of calibration from a reference instrument to another instrument, regardless of the absolute accuracy of the reference.

### 7.2 Noiseless Data:

7.2.1 For clarity, we first consider the case in which the measuring instruments are free of noise. We define vectors n and m as:

$$n = \begin{bmatrix} X \\ Y \\ Z \end{bmatrix} \quad ; m = \begin{bmatrix} X_{\rm m} \\ Y_{\rm m} \\ Z_{\rm m} \end{bmatrix} \tag{7}$$

where:

each is an element of its corresponding vector space, and both derive from the same (a, b, c) setting on a display. The matrix R maps between them:

$$n = R m \,. \tag{8}$$

7.2.2 This relationship may be stated for more than one such pairs of vectors (for multiple display settings) at the same time:

$$N = R M \tag{9}$$

where:

$$N = \begin{bmatrix} X_1 X_2 X_3 \dots X_i \\ Y_1 Y_2 Y_3 \dots Y_i \\ Z_1 Z_2 Z_3 \dots Z_i \end{bmatrix}$$
(10)

and

$$M = \begin{bmatrix} X_{m1} X_{m2} X_{m3} \dots X_{mi} \\ Y_{m1} Y_{m2} Y_{m3} \dots Y_{mi} \\ Z_{m1} Z_{m2} Z_{m3} \dots Z_{mi} \end{bmatrix}$$
(11)

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7.2.3 When matrices N and M have exactly three columns, and when their columns are linearly independent, R may be easily determined:

$$R = N M^{-1} \tag{12}$$

(13)

(14)

The determination of matrix R in this case requires the reference values and the test colorimeter measurements of exactly three distinct colors on the display. In other words, R can be obtained by measuring M for each primary color (red, green, blue) of a display.

7.3 Real-World Transformations of X, Y, Z:

7.3.1 In practice, neither measurements of n nor nor m are made with perfect accuracy. Noise affects the measurements, the linearity presumptions in 6.1.4 and 6.2.3 may not be perfectly true, and there may be other unexpected systematic effects that affect the data. Th One way to reduce such effects of measure; ment imperfection in applying the matrix correction is prudent to determine **R** by using more than three color samples and by using statistical-methods.

7.3.2 For a given  $R_0$  and for a pair of related *n* and *m* vectors:

 $n = R_0 m + v$ 

where:

*n* and *m* are as in Eq 7, and *v* is methods based on the difference vector between the reference tristimulus values *n* and those eomputed least square minimization, as demonstrated by the use of Eq 8. For several different colors, Eq 13 can be expressed as:  $N = R_0 M + V$ 

where: obtaining N is as in Eq 10, *M* is as in Eq 11, and:

	$v_{11} v_{12} v_{13} \dots v_{1i}$	
V =	$v_{21} v_{22} v_{23} \dots v_{2i}$	(15)
	$v_{31}v_{32}v_{33}\cdots v_{3i}$	

7.3.3 When many measurements **n** and **m** are available, the optimal  $R_0$ , hereafter called **R'**, may by measurement of eight colors of a display (Practice E 1455-92). This method, however, was found to be not effective enough to reduce the effect of measuremient noise. This method was improved by minimization applying corrections for the absolute scale of measured tristimulus values for each color of the display, based on the first results from applying Practice E 1455-92, and performing another path of calculation, introducing weights for each color in the minimization processas (Practice E 1455-96). This method improved the performance significantly from the Practice E 1455-92. However, the calculation process has become considerably complicated. Another method has become available, in which the effect of the elements fluctuations of V with respect signals common to all detector chaninels is theoretically elimeinated (9). For example, the effects of measurement errors due to display flicker (causing variation in measured luminance) and instability of display (causing a change of display luminance when reference instrument is measured and when target instrument is measured) are eliminated. This method requires measurements of four colors of a display—each primary color plus white. The R'- matrix is obtained in such a way that the chromaticity errors are reduced to zero for all the four colors, and the correction is valid for all other colors. Correction for Y can also be implemented optionally. This method is theoretically more robust than the statement earlier ASTM methods for correction of least-squares fitting when applied measured chromaticity, and shown to perform equal to or better than Practice E 1455-96, while the -v measurement and calculation process are much simpler. This method (commonly called Four-Color method) is described in the sections below.

7.3.2 Principles of the Method—The primary colors (red, green, and blue) and white of a display are measured by a target instrument (a colorimeter being optimized) and a reference instrument (a calibrated colorimeter or spectroradiometer). From the <u>chromaticity coordinates  $(x_{m,R}, y_{m,R}), (x_{m,G}, y_{m,G}), (x_{m,B}, y_{m,B})$  of red, green, and blue, measured by the target instrument, the</u> relative tristimulus values  $M_{\rm rel RGB}$  of the primary collowrs from the target instrument are expressed as:

$$R' = N \left[ (M M^{T})^{-1} M \right]^{T}$$

$$M_{rel,RGB} = \begin{bmatrix} X_{rel,m,R} & X_{rel,m,G} & X_{rel,m,B} \\ Y_{rel,m,R} & Y_{rel,m,R} & Y_{rel,m,B} \\ Z_{rel,m,R} & Z_{rel,m,G} & Z_{rel,m,B} \end{bmatrix}$$

$$= \begin{bmatrix} x_{m,R} & x_{m,G} & x_{m,B} \\ y_{m,R} & y_{m,G} & y_{m,B} \\ z_{m,R} & z_{m,G} & z_{m,R} \end{bmatrix} \begin{bmatrix} k_{m,R} & 0 & 0 \\ 0 & k_{m,R} & 0 \\ 0 & 0 & k_{m,R} \end{bmatrix}$$

$$where:$$

$$(16)$$

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 $z_{m,R} = 1 - x_{m,R} - y_{m,R}$  $z_{m,G} = 1 - x_{m,G} - y_{m,G}$ 

 $k_{\rm m,R}$ ,  $k_{\rm m,G}$ ,  $k_{\rm m,R}$  are the relative factors to relate the measupred chromaticity coordinates to the relative tristimulus values.

<u>Likewise, from the chromatipcity coordinates ( $x_{r,R}, Ty_{r,R}$ ), ( $x_{r,G}$ , *implies matrix transposition*,  $y_{r,G}$ ), ( $x_{r,R}, y_{r,R}$ ) of red, green, and where we presume that <u>blue measured by</u> the statistical uncertainty (as opposed reference instrument, the relative tristimulus values  $N_{rel,RGR}$  of the primary colors from the reference instrument are expressed as:</u>

	$N_{\mathrm{rel,RGB}} = egin{bmatrix} X_{\mathrm{rel,r,R}} & X_{\mathrm{rel,r,G}} & X_{\mathrm{rel,r,B}} \ Y_{\mathrm{rel,r,R}} & Y_{\mathrm{rel,r,G}} & Y_{\mathrm{rel,r,B}} \ Z_{\mathrm{rel,r,R}} & Z_{\mathrm{rel,r,G}} & Z_{\mathrm{rel,r,B}} \end{bmatrix}$	(14)
	$= \begin{bmatrix} x_{r,R} & x_{r,G} & x_{r,B} \\ y_{r,R} & y_{r,G} & y_{r,B} \\ z_{r,R} & z_{r,G} & z_{r,B} \end{bmatrix} \begin{bmatrix} k_{r,R} & 0 & 0 \\ 0 & k_{r,G} & 0 \\ 0 & 0 & k_{r,B} \end{bmatrix}$	
where:		
	$z_{r,R} = 1 - x_{r,R} - y_{r,R}$ $z_{r,G} = 1 - x_{r,G} - y_{r,G}$ $z_{r,B} = 1 - x_{r,B} - y_{r,B}$	

 $k_{r,R}$ ,  $k_{r,G}$ ,  $k_{r,B}$  are the relative factors to relate the measurement standard uncertainty) measured chromaticity coordinates to the relative tristimulus values.

Based on the additivity of all tristimulus values, when the chromaticity coordinates  $(x_{m,W}, X, Y, Z_{y_{m,W}})$  and  $(x_{r,W}, y_{r,W})$  for white of the display is measured by the target instrument and the reference instrument, respectively, the following relationships hold:

|--|

and

	$\begin{bmatrix} x_{\rm r,W} \\ y_{\rm r,W} \\ z_{\rm r,W} \end{bmatrix}$	=	$\begin{array}{ccc} x_{\mathrm{r,R}} & x_{\mathrm{r,G}} & x_{\mathrm{r,B}} \\ y_{\mathrm{r,R}} & y_{\mathrm{r,G}} & y_{\mathrm{r,B}} \\ z_{\mathrm{r,R}} & z_{\mathrm{r,G}} & z_{\mathrm{r,B}} \end{array}$	$\begin{bmatrix} k_{\rm r,R} \\ k_{\rm r,G} \\ k_{\rm r,B} \end{bmatrix}$	(10
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The white color of the display can be of any intensity combination of the three primary colors. The values of  $\underline{Xk_{m,R}}, \underline{k_{m,R}}, \underline$ 

$k_{m,R}$		$\begin{bmatrix} x_{m,R} & x_{m,G} & x_{m,B} \end{bmatrix}$	$^{-1} [x_{m,W}]$	
$k_{\rm m,G}$	=	y <sub>m,R</sub> y <sub>m,G</sub> y <sub>m,B</sub>	$y_{m,W}$	(17)
$k_{\rm m B}$		ZmR ZmG ZmB	$Z_{\rm m W}$	

and

$k_{r,R}$	1	$x_{r,R} x_{r,G} x_{r,B}$	-1	$x_{r,W}$	
$k_{r,G}$	=	У <sub>г,R</sub> У <sub>г,G</sub> У <sub>г,B</sub>		$y_{r,W}$	(18)
$k_{r,B}$		Z <sub>r,R</sub> Z <sub>r,G</sub> Z <sub>r,B</sub>		$Z_{r,W}$	

By entering the presumption values of identical statistical weights (uncertainties) for each data sample. When R' is used for  $\underline{k}_{m,R}$ ,  $R\underline{k} - \theta_{m,G}$ ,  $\underline{k}_{m,R}$  in Eq. 14, the residuals and V may be examined for trends that might indicate systematic effects.

7.4 Real-World Transformations of Y, x, y:

7.4.1 Eq 16 is the principal result of Wagner (4). However, there is an important situation in which all of X, Y, Z and  $X_{\underline{k}_{m_{\underline{n}\underline{k}}}}$ ,  $\underline{k}_{\underline{r},G}$ ,  $k_{\underline{r},B}$  into Eq 13 and 14,  $M_{rel,RGB}$  and  $N_{rel,RGB}$  are determined, then, the correction matrix  $\mathbf{R}_{rel}$  is obtained by:

$$\mathbf{R}_{\rm rel} = N_{\rm rel,RGB} \cdot \mathbf{M}_{\rm rel,RGB}^{-1} \tag{19}$$

If luminance value Y is not available or of no interest,  $\mathbf{R}_{rel}$  is used to correct the chromaticity coordinates  $(x_m, Zy_m - are not known with equal uncertainties. Many commercial instruments report Y, x, y instead) of X, Y, Z, where:$ 

 $x = \frac{X}{X + Y + Z}; y = \frac{Y}{X + Y + Z}.$  (17)

(We have dropped the m subscripts in Eq 17 for clarity.)

7.4.2 In order for this practice to apply, the instrument must transform *X*, *Y*, *Z* to *Y*, *x*, *y* accurately (internally, in the colorimeter). Instruments with analog circuits that only approximate Eq 17 are not covered.

7.4.3 One may not simply convert *Y*, *x*, *y* to *X*, *Y*, *Z* and proceed as in 7.3. Instruments typically report *x*, *y* to a limited precision. Transformations any color of *Y*, *x*, *y* back to *X*, *Y*, *Z* do not preserve the statistical uncertainties needed for display measured by the data fitting.

7.4.4 Calculation of R' for target instrument. In this case cannot be done as compactly as it was in Eq 16. Instead, we must calculate it a row at a time. Expressing R' as its individual matrix elements, and showing its rows,

$$\frac{R'}{R'} = \begin{bmatrix} R'_{XX} R'_{XY} R'_{XZ} \\ R'_{YX} R'_{YY} R'_{YZ} \\ R'_{ZX} R'_{ZY} R'_{ZZ} \end{bmatrix}$$
(18)



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7.4.5 Calculation case, the relative tristimulus values of the middle row measured color is much the same as in 7.3. taken as:

$$(R'_{YX}R'_{YY}R'_{YZ}) = N_Y [(M_Y M_Y^T)^{-1} M_Y]^T,$$
(19)

where:

$$N_Y = (Y_1 \, Y_2 \, Y_3 \dots Y_i) \,, \tag{20}$$

and

$$- M_{Y} = \begin{bmatrix} X_{m1} X_{m2} X_{m3} \dots X_{m} - y_{m} \end{bmatrix}$$
(21)  
$$MM_{rel} = \begin{bmatrix} X_{rel,m} \\ Y_{rel,m} \\ Z_{rel,m} \end{bmatrix} = \begin{bmatrix} x_{m} \\ y_{m} \\ (1 - x_{m} - y_{m}) \end{bmatrix}$$
(20)

Then the corrected relative tristimulus values  $M'_{\rm rel}$  of the measured color is obtained by:

$$\boldsymbol{M'}_{\text{rel}} = \begin{bmatrix} \boldsymbol{X'}_{\text{rel,m}} \\ \boldsymbol{Y'}_{\text{rel,m}} \\ \boldsymbol{Z'}_{\text{rel,m}} \end{bmatrix} = \boldsymbol{R}_{\text{rel}} \cdot \boldsymbol{M}_{\text{rel}}$$
(21)

The corrected chromaticity coordinate is obtained by:

$$\begin{bmatrix} x'_{m} \\ y'_{m} \end{bmatrix} = \begin{bmatrix} X'_{rel,m} / (X'_{rel,m} + Y'_{rel,m} + Z'_{rel,m}) \\ Y'_{rel,m} / (X'_{rel,m} + Y'_{rel,m} + Z'_{rel,m}) \end{bmatrix}$$
(22)

If the luminance values for the four colors  $(Y_{m,R}, Y_{m,G}, Y_{m,R}, Y_{m,W})$  and  $(Y_{r,R}, Y_{r,G}, Y_{r,B}, Y_{r,W})$  are also measured by the target instrument and the reference instrument, respectively, a correction matrix can be obtained for correction of absolute tristimulus values. In this case, The matrix  $\mathbf{R}_{rel}$  needs only to be scaled by an additional factor.

First, the absolute tristimulus values of the four colors measured by the target instrument are obtained by:

$$M_{R} = \begin{bmatrix}
 Y_{m1} Y_{m2} Y_{m3} \dots Y_{mi} \\
 Z_{m1} Z_{m2} Z_{m3} \dots Z_{mi}
 \end{bmatrix}
 (as in Eq 11),$$

$$M_{R} = \begin{bmatrix}
 X_{m,R} \\
 Y_{m,R} \\
 Z_{m,R}
 \end{bmatrix} = \frac{Y_{m,R}}{y_{m,R}} \cdot \begin{bmatrix}
 x_{m,R} \\
 y_{m,R} \\
 (1 - x_{m,R} - y_{m,R})
 \end{bmatrix}$$

$$M_{G} = \dots$$
with

$$\underline{X}_{mi} = \underline{Y}_{mi} \frac{X_{mi}}{y_{mi}}, \ \underline{Z}_{mi} = \underline{Y}_{mi} \frac{(1 - x_{mi} - y_{mi})}{y_{mi}}.$$
(22)

 $M_{\rm B} = ....$ 

7.4.6 It is useful to compute

$$-(Y'_{1}Y'_{2}Y'_{3}\dots Y'_{i}) = (R'_{YX}R'_{YY}R'_{YZ})M_{Y},$$
(23)

 $M_{\rm W} = \dots$ 

where:

<u>Y'are</u>

Then, the best-fit luminances ratios of the sample display settings.

In some circumstances it is better to use Y' rather than values measured by the reference instrument to the Y' values in computing values measured by the remaining elements of target instrument and corrected by R'. For example, in R rel matrix are obtained by:

$K_R = \frac{Y_{\mathrm{r,R}}}{R_{\mathrm{rel}2} \cdot M_{\mathrm{R}}}$	(24)
$K_{\rm G} = \dots$	
$K_{\rm B} = \dots$	
$K_W = \dots$	

where:

 $\underline{R}_{rel,2}$  is the process second row of computing x, y $\underline{R}_{rel}$  matrix. The from X, Y, Z, an instrument reduces the effects of display flicker in the data. Use  $\underline{R}$  matrix for correction of Y' maintains this noise reduction in the subsequent data fits. On the other hand, if some aspect (and absolute tristimulus values) is then obtained by:

$$\boldsymbol{R} = \frac{(K_{\rm R} + K_{\rm G} + K_{\rm B} + K_{\rm W})}{4} \cdot \boldsymbol{R}_{\rm rel}$$
(25)

When any color of the display is-varying slowly in time, or actually varies based on measured with the display setting, then it

may be better to use *Y* rather than *Y'* values in order to make target instrument, the best comparisons between individual readings of the two instruments. Although the equations in the following sections measured absolute tristimulus values are written with *Y'* rather than *Y*, both versions of the formulae should be considered.

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7.4.7 With statistical weighting, obtained by:

$$N_{X} = \begin{pmatrix} Y'_{1} \frac{x_{1}}{y_{1}} Y'_{2} \frac{x_{2}}{y_{2}} Y'_{3} \frac{x_{3}}{y_{3}} & Y'_{i} \frac{x_{i}}{y_{i}} \\ \sigma_{X1} & \sigma_{X2} & \sigma_{X2} & \sigma_{X3} & \cdots & \sigma_{Xi} \end{pmatrix}$$
(24)

and-

(25) MX = X m1σX1 Xm2 σX2 Xm3σ X3... X miσXiYm1σX1 Ym2σ X2 Ym3 σX3... YmiσXi Zm1σ X1 Zm2 σX2 Zm3σ X3... Z miσ

Ideally we would know the actual statistical uncertainties  $\sigma_{Xi}$ , but we consider the situation in which the two instruments (reference and test) both report x, y to  $\pm$  a constant, such as 0.001. In this case, the measurement precision is limited by the truncation and rounding to three digits. Following the standard rules for propagation of uncertainties, the relative statistical uncertainties are

$$\sigma_{Xi} = Y'_{i} \frac{x_{i}}{y_{i}} \sqrt{\left(\frac{\Delta x}{x_{i}}\right)^{2} + \left(\frac{\Delta y}{y_{i}}\right)^{2} + \left(\frac{\Delta Y}{Y'_{i}}\right)^{2}},$$
(26)

 $(25) \quad MX = (26) \quad M = X \mathrm{m} Y \mathrm{m} Z \mathrm{m}$ 

Ideally we would know the actual statistical uncertainties  $\sigma_{Xi}$ , but we consider the situation in which the two instruments (reference and test) both report x, y to  $\pm$  a constant, such as 0.001. In this case, the measurement precision is limited by the truncation and rounding to three digits. Following the standard rules for propagation of uncertainties, the relative statistical uncertainties are

$$\sigma_{Xi} = Y'_{i} \frac{x_{i}}{y_{i}} \sqrt{\left(\frac{\Delta x}{x_{i}}\right)^{2} + \left(\frac{\Delta y}{y_{i}}\right)^{2} + \left(\frac{\Delta Y}{\overline{Y'_{i}}}\right)^{2}},$$
(26)

where  $\Delta x$ ,  $\Delta y$  (and later,  $\Delta z$ ) are taken as 0.001 (for the sake of example, as these are roughly the standard uncertainties that might be expected in this situation), and  $\Delta Y$  is taken as the experimental standard deviation of the set of values { $(Y'_i - Y_i)$ }. From this, we can calculate as follows:

$$(R'_{XX}R'_{XY}R'_{XZ}) = N_X [(M_X M_X^T)^{-1} M_X]^T,$$
(27)

7.4.8 Similarly,

$$N_{Z} = \left(\frac{Y'_{1}\frac{z_{1}}{y_{1}}Y'_{2}\frac{z_{2}}{y_{2}}Y'_{3}\frac{z_{3}}{y_{3}}}{\sigma_{Z^{2}}\frac{\sigma_{Z^{2}}}{\sigma_{Z^{3}}}\frac{Y'_{i}\frac{z_{i}}{y_{i}}}{\sigma_{Z^{i}}}\right)$$
(28)

and-

$$M_{Z} = \begin{bmatrix} \frac{X_{m1}}{\sigma_{Z1}} \frac{X_{m2}}{\sigma_{Z2}} \frac{X_{m3}}{\sigma_{Z3}} \cdots \frac{X_{mi}}{\sigma_{Zi}} \\ \frac{Y_{m1}}{\sigma_{Z1}} \frac{Y_{m2}}{\sigma_{Z2}} \frac{Y_{m3}}{\sigma_{Z3}} \cdots Y \end{bmatrix}$$
(29)

$$M_{Z} = \begin{bmatrix} X_{\mathrm{m1}} & X_{\mathrm{m2}} & X_{\mathrm{m3}} \\ \overline{\sigma_{Z1}} & \overline{\sigma_{Z2}} & \overline{\sigma_{Z3}} & \dots & \overline{\sigma_{Zi}} \end{bmatrix} = \frac{Y_{\mathrm{m}}}{y_{\mathrm{m}}} = \begin{bmatrix} x_{\mathrm{m}} \\ y_{\mathrm{m}} \\ (1 - x_{\mathrm{m}} - y_{\mathrm{m}}) \end{bmatrix}$$
(29)

The corrected tristimulus values are obtained by:

$$\underline{M}' = [\underline{X'}_{mi}\sigma_{\underline{Z}_i} \frac{\underline{Z}_{m1}}{\sigma} = \underline{R} \cdot \underline{M}$$
(27)

$$\boldsymbol{M}' = \begin{bmatrix} \boldsymbol{X}'_{\mathrm{m}} \\ \boldsymbol{Y}'_{\mathrm{m}} \\ \boldsymbol{Z}'_{\mathrm{m}} \end{bmatrix} = \boldsymbol{R} \cdot \boldsymbol{M}$$
(27)

The corrected chromaticity coordinate is obtained by:

(28)  $x' Z1 Zm2 \sigma Z2 Zm3\sigma Z3 \dots Zmi\sigma Zi$ 

where:

$$z_i = 1 - x_i - y_i, \sigma_{Zi} = Y'_i \frac{z_i}{y_i} \sqrt{\left(\frac{\Delta z}{z_i}\right)^2 + \left(\frac{\Delta y}{y_i}\right)^2 + \left(\frac{\Delta Y}{Y'_i}\right)^2}, \tag{30}$$

 $\underbrace{(28)}_{x'm} x'm = X'm / X'm + Y'm + Z'm Y'm / X'm + Y'm + Z'm$ 

where:

$$z_i = 1 - x_i - y_i, \sigma_{Zi} = Y'_i \frac{z_i}{y_i} \sqrt{\left(\frac{\Delta z}{z_i}\right)^2 + \left(\frac{\Delta y}{y_i}\right)^2 + \left(\frac{\Delta Y}{Y'_i}\right)^2}, \tag{30}$$

# $(R'_{ZX}R'_{ZY}R'_{ZZ}) = N_Z [(M_Z M_Z^T)^{-1} M_Z]^T,$

(31)

### 8. Application

8.1 *Manual OptimizationOptimization*:

8.1.1 The optimization-of\_using this method requires a tristimulus target instrument (a colorimeter requires knowing the true CIE tristimulus values being optimized) and a reference colorimeter that measure chromaticity coordinates (x, y) and, optionally, luminance X, Y, ZY. A correction matrix of at least seven colors R or  $R_{rel}$  is obtained by this method that can be presented on correct the display, three of which must be linearly independent. It is recommended results measured by the target instrument into the results that these colors would be measured by the brightest red, green, blue, yellow, cyan, magenta, and white that reference instrument. The accuracy of the display normally produces. Their tristimulus values corrected results, therefore, depends on the accuracy of measurement by the reference instrument. The reference colorimeter must be determined by a well-trusted instrument, such as a spectroradiometer being used according to Test Method E 1336, or a tristimulus colorimeter with a much closer match to the CIE  $\bar{x}$  ( $\lambda$ ),  $\bar{y}$  ( $\lambda$ ),  $\bar{z}$  ( $\lambda$ ) functions than the colorimeter being optimized. These values are entered into matrix N, following Eq 10:

8.1.2 Measurements are made of these colors with the optimized, or a tristimulus colorimeter <u>b</u> whose relative spectral respongsivity is known and spectral mismatch correctizion is applied.

<u>8.1.2</u> The calibration needs to be v done using the same type of displuay that is measured by the target colorimeter, in order for this method to be effective. The reduction of errors will not be effective if the optimizatrix on is done using one type of display and the obtained M, following Eq. 11.

8.1.3 Matrix R' or R<sub>rel</sub> matrix is computed, following Eq. 16.

8.1.4 If only used for measurement of other types of display X, Y, Z(10) data are available, rather than X, Y, Z data, then. If the analogous steps in 7.4 are followed instead.

8.1.5 Subsequent measurements made by the same tristimulus target colorimeter on is to measure multiple types of displays (for example, CRT, LCD, etc.), the same display are converted using Eq 8, where  $\mathbf{R}'$  is or  $\mathbf{R}_{rel}$  matrix must be obtained for each type of display. The display used for optimization using this method must produce each primary color (red, green, blue) and white. The intensity of each color can be independent with each other, but needs to be stable during each measurement session when the color is measured by both the target instrument and the reference instrument.

<u>8.1.3</u> Measurements of chromaticity coordinates (and luminance Y) are made of the four colors with the target colorimeter and the reference instrument. These values are entered into Eq 17 and 18 to obtain  $k_{m,R}$ ,  $k_{m,G}$ ,  $k_{m,B}$  and  $k_{r,R}$ ,  $k_{r,G}$ ,  $k_{r,B}$  and then to calculate matrix  $\mathbf{R}_{rel}$  in Eq 19. If there are no luminance (Y) data, optimization is complete.

8.1.4 If there are luminance (Y) data, these are entered into Eq 23 and 24 to calculate matrix R. The resultant n vector is taken as the optimized (adjusted) result of the measurement. in Eq 25.

8.2 A<u>Manual Data Correction</u>—Subsequent measurements made by the same tristimulus c-Oolorimeter on the same display are corrected using Eq 20-22 when there is no lumiznance data, or using Eq 26-28 when luminance data are included.

8.3 Automatic Data correction:

8.23.1 All tristimulus colorimeters have, in some form, an internal calibration matrix C that relates detector signals to tristimulus values, as described in Eq 2. C may be required to reduce the dimensionality of the instrument from f to 3.

8.23.2 A tristimulus colorimeter may, by design, incorporate a provision to transform a tentative determination of *X*, *Y*, *Z* (that is,  $X_m$ ,  $Y_m$ ,  $Z_m$ ) to a more accurate determination of *X*, *Y*, *Z* by the application of Eq 8. Such a colorimeter contains, in some form, an embodiment of matrix *R*. This matrix is distinguished from the *C* matrices shown in Eq 3-5 by the fact that it contains, in general, no zero elements. That is, all three inputs contribute to the determination of all three tristimulus values, with nine degrees of calibration freedom. *EC and and R may be implemented jointly.* 

8.23.3 A tristimulus colorimeter may be described as compatible with this standard practice if and only if (I) (1) it includes an implementation of matrix  $\mathbf{R}$  or  $\mathbf{R}_{rel}$ , and (2) (2) the user of the colorimeter has means to set the nine  $\mathbf{R}\mathbf{R}$  or  $\mathbf{R}_{rel}$  matrix elements to allow continued, automatic application of Eq 8. A compaftible colorimether may also provide means to compute  $\mathbf{R}'$  matrix has been determined. A compatible colorimeter may also provide means to compute  $\mathbf{R}'\mathbf{R}_{rel}$  by allowing the user to enter the true X, Y, Z of at least seven (x, y) or (x, y, Y) of each primary color samples. and white of a display. These implementations may be either locally dedicated to the colorimeter or installed in a computer interfaced to the colorimeter.

### 9. Precision and Bias

9.1 The typical precision and bias of tristimulus value measurements made using this practice have yet to be determined. However, it is expected that the limits of precision and the origins of bias in such measurements will arise from causes outside of the scope of this practice, such as those discussed as follows:

9.1.1 This practice transfers the calibration from a well-trusted spectroradiometer or a colorimeter to another instrument, a tristimulus colorimeter. No matter how well the transfer is made, the bias of the final measurements will reflect the precision and bias of the reference device.

9.1.2 This practice is limited to discussion of the spectral characteristics of the instruments and does not consider any biases that might arise from the geometry of collection of radiant flux by either the tristimulus colorimeter or the reference device. For

example, the spectral radiance of an active matrix liquid crystal-(AMLCD) display-is (AMLCD) can be highly directional.-<u>S</u> Care <u>must be taken when such a display-could not be is</u> used to transfer calibration between instruments with different numerical apertures. Also, displays exhibit spatial nonuniformities in their radiance. The inability of dissimilar instruments to measure the same area of a display can also limit the accuracy of this technique.

9.1.3 <u>TWhile this practice does not consider relives the effect of the</u> temporal response characteristics of <u>either</u> the tristimulus target colorimeter or the reference device. <u>T (for example, against flicker of displays)</u>, the user is reminded that <u>many types of displays are scanned</u>, and the <u>correction of luminance values (using Eq 27) is still liable to measurement errors due to display</u> flicker-may impart a bias, and instability, particularly if the colorimeter and the reference device instrument are dissimilar.

9.1.4 This practice presumes linear instrumental and display behavior, as described in 6.1.4 and 6.2.3. The measurements may be biased if these presumptions are incorrect.

9.1.5 This practice does not consider biases that might arise due to the environment in which it is performed. Specifically, ambient light may affect the measurements if they are not made in a dark room. Changes in ambient temperature may affect the performance of either the tristimulus colorimeter or the reference device.

9.1.6 The selection of the filter passbands (6.1.1) and the selection of the  $C_{ij}$  matrix elements when f > 3 (6.1.3-6.1.6) are topics beyond the scope of this practice. However, these These choices affect the precision of the technique by emphasizing or deemphasizing statistically significant differences between the detector channel signals that correlate to the differences in the tristimulus values of the light source. However, effects such as bandpass and wavelengh errors of a spectroradiometer contribute to distorted color matching functions when tristimulus values are calculated from the spectral data, in which case, this ASTM method is effective, often for array-type spectroradiometers.

9.2 This practice is intended to help minimize the errors in the determination of the tristimulus values X, Y, Z. chromaticity coordinates (x, y) or (u', v'). No representation is made that this practice minimizes errors in the determination of chromaticity coordinates x, y or u, v, perceptible color differences, or any other values computed from X, Y, Z. absolute tristimulus values.

### 10. Keywords

10.1 calibration (tristimulus colorimeters); cathode ray tubes (CRTs); chromaticity; CIE color-scale system; CIE tristimulus values; color; choromaticity coordinates; colorimetry; data analysis; flat-panel displays; instrumental measurement (color/light); liquid crystal displays (LCDs); luminance; matrix transformation; self-luminous displays; tristimulus colorimeters; tristimulus values; visual/video display units (VDUs)

### APPENDIX

### (Nonmandatory Information)

### **X1. NUMERICAL EXAMPLE**

X1.1 A numerical example of the optimization procedure is given here for the case in which the chromaticity coordinates (rather than the tristimulus values) are known.

X1.2 A CRT is made to display eight elementary and luminance of 10 colors (more than the minimum required number of seven). Each color is a CRT display were measured by two colorimeters, with a target instrument (a tristimulus colorimeter) and a reference instrument (a spectroradiometer), and the instrument being optimized (the target). The data are given optimization procedure described in this ASTM standard practice was applied. Table X1.1-

X1.3 The reference luminance (Y) values are arranged in shows the form of a  $1 \times 8 N_Y$  matrix, as in Eq 20. The target data are converted from Y, x, y to X, Y, Z format ( $X_m$ ,  $Y_m$ ,  $Z_m$ ) using Eq 22, and matrix  $M_Y$  is constructed with eight columns as in Eq 21. The middle row of the R' matrix (Eq 18) is computed using Eq 19.

X1.4 Using  $M_{Y'}$  and the results of the previous step, the best-fit Y are computed using Eq 23. These results are also shown in Table X1.1. The rms difference between the corresponding reference Y and Y' values is 0.125, which is taken to be  $\Delta Y$  in the following steps.

X1.5 For each of the eight samples, an uncertainty  $\sigma_{Xi}$  is computed using Eq 26. This computation uses the best-fit Y' determined in X1.4, the reference x, y from Table X1.1,  $\Delta$  Y as determined in X1.4, measurements and 0.001 corrections for  $\Delta x$  and  $\Delta y$ . The values 0.001 are adopted because the instruments in this example report chromaticity coordinates (x, y to  $\pm 0.001$ .

X1.6 Matrix  $N_X(\text{Eq 24})$ , one row of eight columns, is constructed using the reference x, y data in). Table X1.1 and X1.2 shows the results of the previous two steps. Matrix  $M_X$  (Eq 24), three rows of eight columns, is constructed using the uncertainties computed in X1.5 measurements and the corrections for luminance  $X_m$ , Y - m,  $Z_m$  computed in X1.4... The top row of the obtained R<u>R</u>-matrix (Eq 18) is computed using Eq 27.

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X1.7 For each of the eight samples, an uncertainty  $\sigma_{Zi_{rel}}$  is computed using Eq 30. This computation parallels that in X1.5.

X1.8 Matrices  $N_Z$  (Eq 28) matrix and  $M_{\overline{R}_Z}(Eq 29)$  are constructed analogous to the way  $N_X$  and  $M_X$  were in X1.6. The bottom row of the R' matrix (Eq 18) is computed using Eq 31.

Elementary —CRT	Referen	ce <u>Inst.</u>	Targe	t Inst	<del>Y′</del> Ori Erro	ginal ors	Correcte	d Target Inst.	Residua	al Error
Color	+ <u>x</u>	<u>y</u>	X	У	$\Delta \Upsilon x$	$\Delta y$	X	У	$\Delta x$	$\Delta y$
Full White Red Green Green Yellow Blue Blue Cyan Magenta Magenta	$\begin{array}{r} 0.3232\\ \hline 12.25\\ 0.6300\\ \hline 38.45\\ 0.3109\\ \hline 50.85\\ 0.1503\\ \hline -6.43\\ 0.2344\\ \hline 18.65\\ 0.3277\end{array}$	$\begin{array}{r} 0.3395\\ \hline 0.617\\ \hline 0.3354\\ \hline 0.294\\ \hline 0.5927\\ \hline 0.409\\ \hline 0.0633\\ \hline 0.150\\ \hline 0.3410\\ \hline 0.286\\ \hline 0.1629\\ \end{array}$	$\begin{array}{r} 0.322\\ \hline 0.351\\ \hline 0.632\\ \hline 0.604\\ \hline 0.306\\ \hline 0.516\\ \hline 0.144\\ \hline 0.075\\ \hline 0.232\\ \hline 0.154\\ \hline 0.330\\ \end{array}$	$\begin{array}{r} 0.347\\\hline 11.50\\0.335\\\hline 36.25\\0.592\\\hline 47.53\\0.061\\\hline -5.11\\0.352\\\hline 16.43\\0.165\\\hline \end{array}$	$\begin{array}{r} -0.0012 \\ \hline 0.620 \\ \hline 0.0020 \\ \hline 0.293 \\ \hline 0.0049 \\ \hline 0.413 \\ \hline 0.0063 \\ \hline 0.153 \\ \hline 0.0024 \\ \hline 0.293 \\ \hline 0.0023 \end{array}$	0.0075 0.350 -0.0004 0.605 -0.0007 0.514 -0.0023 0.070 0.0110 0.153 0.0021	0.3232 -12.6300 0.6300 38109 -503 0.1503 -6.341 0.2341 -184 0.3281	$\begin{array}{c} \underline{0.3395} \\ \hline 0.3354 \\ \hline 0.47 \\ \hline 0.5927 \\ \hline 0.6433 \\ \hline 0.0633 \\ \hline 0.3422 \\ \hline 0.3422 \\ \hline 0.3422 \\ \hline 0.551637 \\ \hline 0.1637 \end{array}$	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0003 0.0003 0.0004	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00012 0.0012 0.00012 0.0008
Color 8 Gray Color 9 Color 110	44.70 0.4256 56.75 0.3735 11.90 0.3207 -0.817	0.211 0.5025 0.289 0.3406 0.297 0.4069 0.2740	0.301 0.420 0.311 0.373 0.323 0.318 0.280	41.25 0.504 52.55 0.347 10.95 0.415 -0.281	-0.213 -0.0056 -0.293 -0.0005 -0.302 -0.0027 -0.0017	0.299           0.0015           0.309           0.0064           0.320           0.0081           0.0070	<u>44.74255</u> 0.4255 <u>56.93738</u> 0.3738 <u>0.3204</u> 0.3204 <u>0.2810</u>	0.5023 0.5023 0.3408 0.3408 0.4078 0.4078 0.4078 0.2735	-0.0002 -0.0002 -0.0003 -0.0003 -0.0004 -0.0004 -0.0007	-0.0002 -0.0002 -0.0002 -0.0009 -0.0009 -0.0009 -0.0005
Color 10 RMS	0.2817	<u>0.2740</u>	0.280	0.281	<u>-0.0017</u> 0.0035	0.0070	0.2810	0.2735	<u>-0.0007</u> 0.0003	<u>-0.0005</u> 0.0006

### TABLE X1.1 EResults for Measuremient ancd Corre actiond of Chromaticity Coordinates of Eight Sample Colors (x, y)

### TABLE X1.2 AppResulicatis for Measuremen of Optimiz and Correction Transf orf Lum to Rinaw Datance Y

		Ta <u>Colo</u> r <del>get</del>			Optimized Target			
CR <del>eference</del>	$\neq$	*Ref.	∀Test	<b></b> <b>Y</b> Original	*Corrected	-		
<u>-</u>		Inst. Y	Inst. Y	Error	lest	<del>y</del> Re		
					Inst.			
(cd/m <sup>2</sup> )	¥	¥	<del>y (cd/</del>	(%)				
(64/11)	•	~	<del>m<sup>2</sup>)</del>	(70)				
(cd/m <sup>2</sup> )	(cd/m <sup>2</sup> )	(%)	(cd/m <sup>2</sup> )	<u>(%)</u>				
36.10	<del></del>	<del></del>	<del>33.00</del>	<del></del>	 <del>0.256</del>			
Full	163.43	164.0	0.4	162.99	-0. <del>256</del>			
White								
<del>36.05</del>	<del>- 0.236</del>	<del></del>						
Red	36.01	35 <del>8</del>						
<del>17</del> .70	0.551	0.404	16.556					
17.6	1.1	36.22	0.6					
Green	<del>- 0.556</del>	<del></del>	<del>17.76</del>	<del></del>				
Green	120.46	123.0	2.1	120.22	-0.2			
-5.82	<u>-0.314</u>	— <u>0.573</u>	-5.49	<u>-0.315</u>	— <u>0.576</u>			
Blue		10.8	-9.5		<u>-0.576</u>			
<del>28.50</del>		<u>-0.216</u>	<del>25.85</del>	<u>-0.262</u>	<u>-0.215</u>			
Cyan	<u>130.53</u>	<u>133.0</u>	1.9	<u>131.30</u>	<u>0.215</u>			
<del>16.90</del>			15.10					
Magenta	46.41	45.4	-2.2	47.09	185			
12.00			11.95		0.350			
12.20	<u>131.11</u> 0.200	155.0	2.0	0.208	0.22412.19			
Color 8	104.28	105.0	0.7	104.72	0.412.10			
40.20	0.218	0585	27.70	0.318				
Color 9	142 07	145.0	21	143 17	0.85			
-5.59	0.295	-0.587	-5.27	-0.294	<u>-0.591</u>			
Color	94.00	94.9	1.0	94.83	0.9 <del>1</del>			
10								
<del>10.10</del>	-0.481		-9.35	-0.488				
RMS			3.4		<u> </u>			

X1.9 In in this example, example are:

<u>ل</u> E 1455 – <del>97</del> 03	
$\boldsymbol{R'} = \begin{bmatrix} 1.0536 & 0.0007 & 0.0088\\ 0.0144 & 1.0519 & 0.0138\\ 0.0081 & -0.0080 & 1.0861 \end{bmatrix}$	(X1.1)
$\boldsymbol{R}_{\text{rel}} = \begin{bmatrix} 1.0059 & -0.0181 & 0.0169 \\ 0.0290 & 0.9463 & 0.0055 \\ 0.0171 & -0.0305 & 1.0342 \end{bmatrix}$	(X1.1)

<del>X1.10</del>

		and	
R =	1.0218 0.0294 0.0173	-0.0183 0.9612 -0.0310	0.0172 - 0.0056 - 0.0056 - 0.00505

R' is applied to all subsequent measurements using the target instrument on the same CRT (or perhaps type of CRT) as used for the data in Table X1.1. *Y*, *x*, *y* data from the target instrument, shown in Table X1.2, are converted to *X*, *Y*, *Z* format, multiplied by R' as in Eq 8, and converted back to *Y*, *x*, *y* format. These results are shown in Table X1.2 as the Optimized Target. In this example, the results may be compared to the corresponding readings from the reference instrument, although normally the reference instrument would no longer be used after R' is determined.

### REFERENCES

- (1) Colorimetry, 2nd ed., Publication 15.2, (Commission Internationale de L'Éclairage, Vienna, 1986). (Currently available through the U.S. National Committee of the CIE, c/o Mr. Thomas M. Lemons, TLA-Lighting Consultants, Inc., 7 Pond Street, Salem, MA 01970-4819.)
- (2) Berns, R. S., Gorzynski, M. E., and Motta, R. J., "CRT Colorimetry. Part II: Theory and Practice," *Color Research and Application*, Vol 18, 1993, pp. 315–325.
- (3) Berns, R. S., Motta, R. J., and Gorzynski, M. E., "CRT Colorimetry. Part I: Theory and Practice," *Color Research and Application*, Vol 18, 1993, pp. 299–314.
- (4) Wagner, H. G., "Farbmessungen an Fernseh-Farbbildröhren nach dem Dreibereichsverfahren," ("Color Measurement on Color Television Tubes Using the Three-Range Method,") *Farbe*, Vol 22, 1973, pp. 31–43.
- (5) Lux, G., and Schanda, J., "On the Vectorial Representation of Basic Colour Perception and Its Use in Colour-Measurement," Reports of the Scientific Staff of the Research Institute for Technical Physics of the Hungarian Academy of Sciences, 1974, pp. 5–27.
- (6) Kokoschka, S., "Matrixkorrektur fehlangepaßter Dreibereichsfarbmeßgeräten," ("Matrix Correction of Wrongly Adjusted Tristimulus Colorimeters,") Farbe + Design, No. 11, 1979, pp. 22–25.
- (7) Erb, W., Krystek, M., and Budde, W., "A Method for Improving the Accuracy of Tristimulus Colorimeters," *Color Research and Application*, Vol 9, 1984, pp. 84–88.
- (8) Eppeldauer, G., Schanda, J., Lux, G., "Berendezés szinösszetevök és szinkoordináták meghatározására," ("Instrument to Determine CIE Tristimulus Values and Chromaticity Coordinates,") Hungarian Patent No. 168,258, Feb. 28, 1977 (*Expired*).

(9) Ohno, Y., and Suzuki, R., "Colorimeter Hardis, J., "Improved Matrix Method for Tristimulus Colorimetry of Displays," United States Patent No. 5,363,197, Nov. 8, 1994. Proc., 8th Congress of the International Color Association, AIC Color 97 Kyoto, Vol 2, 1997, pp. 570–573.

(10) Ohno, Y., and Brown, S., "Four-Color Matrix Method for Correction of Tristimulus Colorimeters—Part 2," Proc., IS&T Sixth Color Imaging Conference, 1998, pp. 65–68.

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