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AMERICAN SOCIETY FOR TESTING AND MATERIALS  
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## Standard Test Method for Young's Modulus, Shear Modulus, and Poisson's Ratio for Glass and Glass-Ceramics by Resonance<sup>1</sup>

This standard is issued under the fixed designation C 623; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

<sup>ε1</sup> NOTE—Section 10 was added editorially in April 1995.

### 1. Scope

1.1 This test method covers the determination of the elastic properties of glass and glass-ceramic materials. Specimens of these materials possess specific mechanical resonance frequencies which are defined by the elastic moduli, density, and geometry of the test specimen. Therefore the elastic properties of a material can be computed if the geometry, density, and mechanical resonance frequencies of a suitable test specimen of that material can be measured. Young's modulus is determined using the resonance frequency in the flexural mode of vibration. The shear modulus, or modulus of rigidity, is found using torsional resonance vibrations. Young's modulus and shear modulus are used to compute Poisson's ratio, the factor of lateral contraction.

1.2 All glass and glass-ceramic materials that are elastic, homogeneous, and isotropic may be tested by this test method.<sup>2</sup> The test method is not satisfactory for specimens that have cracks or voids that represent inhomogeneities in the material; neither is it satisfactory when these materials cannot be prepared in a suitable geometry.

NOTE 1—Elastic here means that an application of stress within the elastic limit of that material making up the body being stressed will cause an instantaneous and uniform deformation, which will cease upon removal of the stress, with the body returning instantly to its original size and shape without an energy loss. Glass and glass-ceramic materials conform to this definition well enough that this test is meaningful.

NOTE 2—Isotropic means that the elastic properties are the same in all directions in the material. Glass is isotropic and glass-ceramics are usually so on a macroscopic scale, because of random distribution and orientation of crystallites.

1.3 A cryogenic cabinet and high-temperature furnace are described for measuring the elastic moduli as a function of temperature from  $-195^{\circ}\text{C}$  to  $1200^{\circ}\text{C}$ .

1.4 Modification of the test for use in quality control is

possible. A range of acceptable resonance frequencies is determined for a piece with a particular geometry and density. Any specimen with a frequency response falling outside this frequency range is rejected. The actual modulus of each piece need not be determined as long as the limits of the selected frequency range are known to include the resonance frequency that the piece must possess if its geometry and density are within specified tolerances.

1.5 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

### 2. Summary of Test Method

2.1 This test method measures the resonance frequencies of test bars of suitable geometry by exciting them at continuously variable frequencies. Mechanical excitation of the specimen is provided through use of a transducer that transforms an initial electrical signal into a mechanical vibration. Another transducer senses the resulting mechanical vibrations of the specimen and transforms them into an electrical signal that can be displayed on the screen of an oscilloscope to detect resonance. The resonance frequencies, the dimensions, and the mass of the specimen are used to calculate Young's modulus and the shear modulus.

### 3. Significance and Use

3.1 This test system has advantages in certain respects over the use of static loading systems in the measurement of glass and glass-ceramics:

3.1.1 Only minute stresses are applied to the specimen, thus minimizing the possibility of fracture.

3.1.2 The period of time during which stress is applied and removed is of the order of hundreds of microseconds, making it feasible to perform measurements at temperatures where delayed elastic and creep effects proceed on a much-shortened time scale, as in the transformation range of glass, for instance.

3.2 The test is suitable for detecting whether a material meets specifications, if cognizance is given to one important fact: glass and glass-ceramic materials are sensitive to thermal history. Therefore the thermal history of a test specimen must

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee C-14 on Glass and Glass Products and is the direct responsibility of Subcommittee C14.04 on Physical and Mechanical Properties.

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<sup>2</sup> Spinner, S., and Tefft, W. E., "A Method for Determining Mechanical Resonance Frequencies and for Calculating Elastic Moduli from These Frequencies," *Proceedings, ASTM*, 1961, pp. 1221–1238.

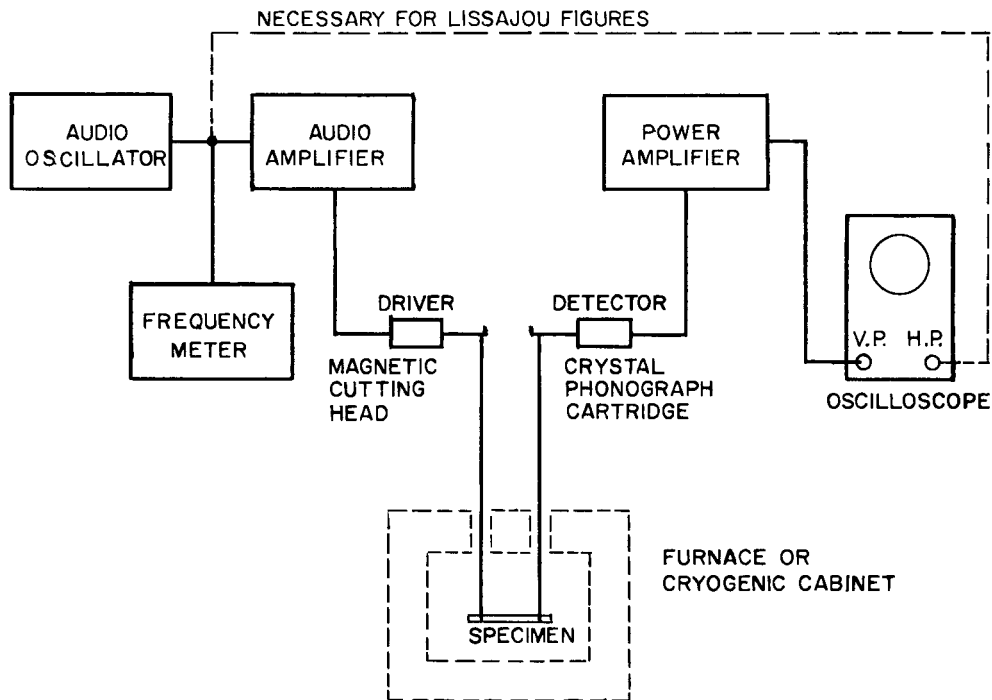


FIG. 1 Block Diagram of Apparatus

be known before the moduli can be considered in terms of specified values. Material specifications should include a specific thermal treatment for all test specimens.

#### 4. Apparatus

4.1 The test apparatus is shown in Fig. 1. It consists of a variable-frequency audio oscillator, used to generate a sinusoidal voltage, and a power amplifier and suitable transducer to convert the electrical signal to a mechanical driving vibration. A frequency meter monitors the audio oscillator output to provide an accurate frequency determination. A suitable suspension-coupling system cradles the test specimen, and another transducer acts to detect mechanical resonance in the specimen and to convert it into an electrical signal which is passed through an amplifier and displayed on the vertical plates of an oscilloscope. If a Lissajous figure is desired, the output of the oscillator is also coupled to the horizontal plates of the oscilloscope. If temperature-dependent data are desired, a suitable furnace or cryogenic chamber is used. Details of the equipment are as follows:

4.2 *Audio Oscillator*, having a continuously variable frequency output from about 100 Hz to at least 20 kHz. Frequency drift shall not exceed 1 Hz/min for any given setting.

4.3 *Audio Amplifier*, having a power output sufficient to ensure that the type of transducer used can excite any specimen the mass of which falls within a specified range.

4.4 *Transducers*—Two are required: one used as a driver may be a speaker of the tweeter type or a magnetic cutting head or other similar device, depending on the type of coupling chosen for use between the transducer and the specimen. The other transducer, used as a detector, may be a crystal or magnetic reluctance type of phonograph cartridge. A capacitive pickup may be used if desired. The frequency response of the transducer shall be as good as possible with at least a 6.5-kHz

bandwidth before 3-dB power loss occurs.

4.5 *Power Amplifier*, in the detector circuit shall be impedance matched with the type of detector transducer selected and shall serve as a prescope amplifier.

4.6 *Cathode-Ray Oscilloscope*, shall be any model suitable for general laboratory work.

4.7 *Frequency Counter*, shall be able to measure frequencies to within  $\pm 1$  Hz.

4.8 If data at elevated temperature are desired, a furnace shall be used that is capable of controlled heating and cooling. It shall have a specimen zone 180 mm in length, which will be uniform in temperature within  $\pm 5^\circ\text{C}$  throughout the range of temperatures encountered in testing.

4.9 For data at cryogenic temperatures, any chamber shall suffice that shall be capable of controlled heating, frost-free, and uniform in temperature within  $\pm 5^\circ\text{C}$  over the length of the specimen at any selected temperature. A suitable cryogenic chamber<sup>3</sup> is shown in Fig. 2.

4.10 Any method of specimen suspension shall be used that shall be adequate for the temperatures encountered in testing and that shall allow the specimen to vibrate without significant restriction. Common cotton thread, silica glass fiber thread, Nichrome, or platinum wire may be used. If metal wire suspension is used in the furnace, coupling characteristics will be improved if, outside the temperature zone, the wire is coupled to cotton thread and the thread is coupled to the transducer. If specimen supports of other than the suspension type are used, they shall meet the same general specifications.

<sup>3</sup> Smith, R. E., and Hagy, H. E., "A Low Temperature Sonic Resonance Apparatus for Determining Elastic Properties of Solids," *Internal Report 2195*, Corning Glass Works, April, 1961.

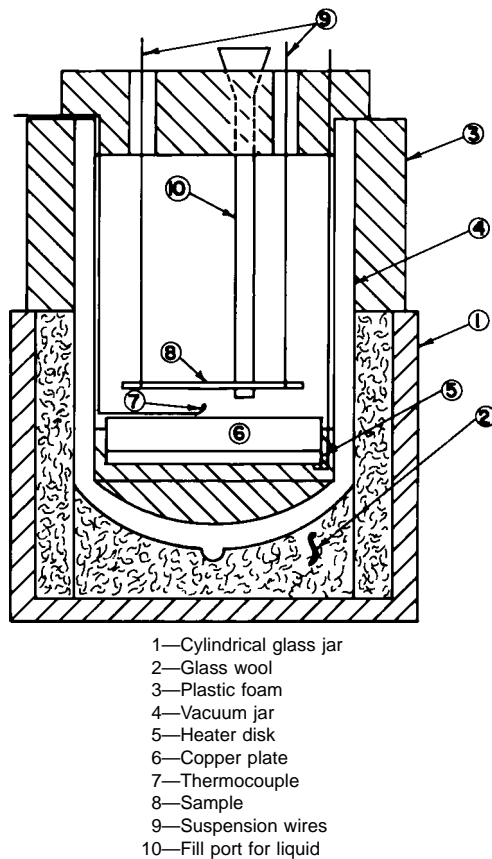


FIG. 2 Detail Drawing of Suitable Cryogenic Chamber

### 5. Test Specimen

5.1 The specimens shall be prepared so that they are either rectangular or circular in cross section. Either geometry can be used to measure both Young's modulus and shear modulus. However, great experimental difficulties in obtaining torsional resonance frequencies for a cylindrical specimen usually preclude its use in determining shear modulus, although the equations for computing shear modulus with a cylindrical specimen are both simpler and more accurate than those used with a prismatic bar.

5.2 Resonance frequencies for a given specimen are functions of the bar dimensions as well as its density and modulus; therefore, dimensions should be selected with this relationship in mind. Selection of size shall be made so that, for an estimated modulus, the resonance frequencies measured will fall within the range of frequency response of the transducers used. Representative values of Young's modulus are  $70 \times 10^4$  kgf/cm<sup>2</sup> (69 GPa) for glass and  $100 \times 10^4$  kgf/cm<sup>2</sup> (98 GPa) for glass-ceramics. Recommended specimen sizes are 120 by 25 by 3 mm for bars of rectangular cross section, and 120 by 4 mm for those of circular cross section. These specimen sizes should produce a fundamental flexural resonance frequency in the range from 1000 to 2000 Hz. Specimens shall have a minimum mass of 5 g to avoid coupling effects; any size of specimen that has a suitable length-to-cross section ratio in terms of frequency response and meets the mass minimum may be used. Maximum specimen size and mass are determined primarily by the test system's energy and space capabilities.

5.3 Specimens shall be finished using a fine grind -400-grit or smaller. All surfaces shall be flat and opposite surfaces shall be parallel within 0.02 mm.

### 6. Procedure

6.1 *Procedure A—Room Temperature Testing*—Position the specimen properly (see Fig. 3 and Fig. 4). Activate the equipment so that power adequate to excite the specimen is delivered to the driving transducer. Set the gain of the detector circuit high enough to detect vibration in the specimen and to display it on the oscilloscope screen with sufficient amplitude to measure accurately the frequency at which the signal amplitude is maximized. Adjust the oscilloscope so that a sharply defined horizontal baseline exists when the specimen is not excited. Scan frequencies with the audio oscillator until specimen resonance is indicated by a sinusoidal pattern of maximum amplitude on the oscilloscope. Find the fundamental mode of vibration in flexure, then find the first overtone in flexure (Note 3). Establish definitely the fundamental flexural mode by positioning the detector at the appropriate nodal position of the specimen (see Fig. 5). At this point the amplitude of the resonance signal will decrease to zero. The ratio of the first overtone frequency to the fundamental frequency will be approximately 2.70 to 2.75. If a determination of the shear modulus is to be made, offset the coupling to the transducers so that the torsional mode of vibration may be detected (see Fig. 3). Find the fundamental resonance vibration in this mode. Identify the torsional mode by centering the detector with respect to the width of the specimen and observing that the amplitude of the resonance signal decreases to zero; if it does not, the signal is an overtone of flexure or a spurious frequency generated elsewhere in the system. Dimensions and weight of the specimen may be measured before or after the test. Measure the dimensions with a micrometer caliper capable of an accuracy of  $\pm 0.01$  mm; measure the weight with a balance capable of  $\pm 10$  mg accuracy.

NOTE 3—It is recommended that the first overtone in flexure be determined for both rectangular and cylindrical specimens. This is useful

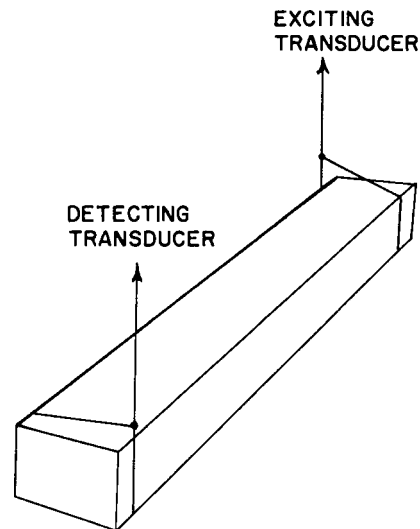


FIG. 3 Specimen Positioned for Measurement of Flexural and Torsional Resonance Frequencies Using Thread or Wire Suspension

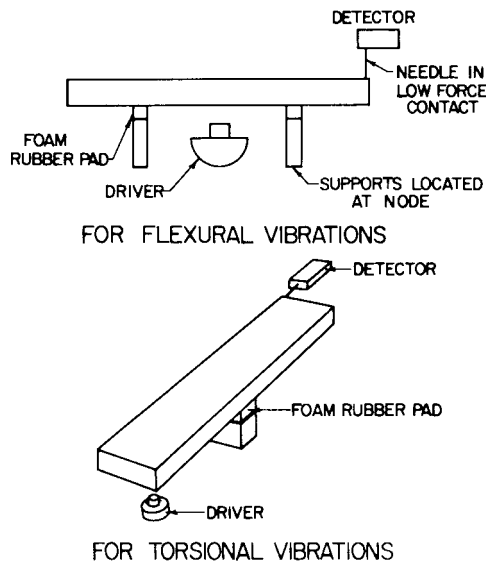


FIG. 4 Specimen Positioned for Measurement of Flexural and Torsional Resonance Frequencies Using “Tweeter” Exciter

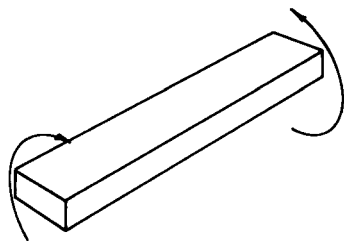
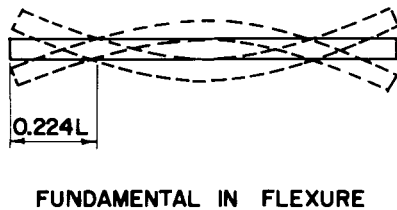


FIG. 5 Some Modes of Mechanical Vibration in a Bar

in establishing the proper identification of the fundamental, particularly when spurious frequencies inherent in the system interfere (as, for example, when greater excitation power and detection sensitivity are required for work with a specimen that has a poor response). The fundamental and overtone are properly identified by showing them to be in the correct numerical ratio, and by demonstrating the proper locations of the nodes for each. Spinner and Tefft recommended using only the fundamental in flexure when computing Young’s modulus for a rectangular bar because of the approximate nature of Pickett’s theory. However, for the nominal size of bar specified, the values of Young’s modulus computed using Eq 1 and Eq 2 will agree within 1 %. When the correction factor,  $T_2$ , is greater than 2 %, Eq 2 should not be used.

6.2 Procedure B—Elevated Temperature Testing— Determine the mass, dimensions, and frequencies at room temperature in air as outlined in 6.1. Place the specimen in the furnace and adjust the driver-detector system so that all the

frequencies to be measured can be detected without further adjustment. Determine the resonant frequencies at room temperature in the furnace cavity with the furnace doors closed, etc., as will be the case at elevated temperatures. Heat the furnace at a controlled rate that does not exceed 150°C/h. Take data at 25° intervals or at 15-min intervals as dictated by heating rate and specimen composition. Follow the change in resonance frequencies with time closely to avoid losing the identity of each frequency. (The overtone in flexure and the fundamental in torsion may be difficult to differentiate if not followed closely; spurious frequencies inherent in the system may also appear at temperatures above 600°C using certain types of suspensions, particularly wire.) If desired, data may also be taken on cooling; it must be remembered, however, that high temperatures may damage the specimen, by serious warping for example, making subsequent determinations of doubtful value.

6.3 Procedure C—Cryogenic Temperature Testing— Determine the weight, dimensions, and resonance frequencies in air at room temperature. Measure the resonance frequencies at room temperature in the cryogenic chamber. Take the chamber to the minimum temperature desired (Note 4), monitoring frequencies as the chamber is cooled. Allow the specimen to stabilize at minimum temperature for at least 15 min. Take data on heating. Heating rate should not exceed 50°C/h and data may be taken at intervals of 10 min or 15°C or as desired.

NOTE 4—Precautions should be taken to remove water vapor from the chamber by flushing the dry nitrogen gas prior to chilling so that frost deposits on the specimen do not cause anomalous results.

7. Calculation

7.1 Young’s Modulus:

7.1.1 For the fundamental in flexure of a rectangular bar (Note 5):

$$E = 96.517 (L^3/br^3)T_1wf^2 \times 10^{-8} \tag{1}$$

where:

- $E$  = Young’s modulus, kgf/cm<sup>2</sup>,
- $L$  = length of the bar, cm,
- $b$  = width of the bar, cm,
- $t$  = thickness of the bar, cm
- $w$  = weight of the bar, g,
- $f$  = resonance frequency of bar, Hz, and
- $T_1$  = correction factor for fundamental flexural model to account for finite thickness of bar, Poisson’s ratio, etc. (See Table 1 for a plot of  $T_1$  as a function of bar dimensions and Poisson’s ratio.)

NOTE 5—Pickett and Goens have analyzed the relationship of the general equation for modulus of elasticity:

$$M = Kw_Mf_M^2$$

where:

- $M$  = elastic modulus,
- $K$  = factor whose value depends on the dimensions of the bar and the particular characteristic vibration being investigated,
- $w$  = weight of the bar, and
- $f_M$  = frequency, Hz, of the characteristic vibration.

From this equation they have developed specific equations for use in the flexural and torsional modes of vibration (Eq 1 Eq 2 Eq 3 Eq 4 Eq 5 Eq

**TABLE 1 Correction Factor,  $T_1$ , for the Fundamental Mode of Flexural Vibration**

$K (t/L)^A$	Poisson's Ratio			
	0.15	0.20	0.25	0.30
0.000	1.000000	1.000000	1.000000	1.000000
0.005	1.002029	1.002053	1.002077	1.002100
0.010	1.008102	1.008199	1.008295	1.008388
0.015	1.018186	1.018405	1.018619	1.018826
0.020	1.032233	1.032618	1.032994	1.033360
0.025	1.050174	1.050765	1.051344	1.051916
0.030	1.071920	1.072753	1.073577	1.074393
0.035	1.097378	1.098495	1.099599	1.100694
0.040	1.126452	1.127884	1.129302	1.130711
0.045	1.159039	1.160817	1.162582	1.164337
0.050	1.195038	1.197191	1.199332	1.201464
0.055	1.234351	1.236906	1.239449	1.241986
0.060	1.276886	1.279865	1.282836	1.285807
0.065	1.322555	1.325980	1.329403	1.332832
0.070	1.371276	1.375167	1.379065	1.382977
0.075	1.422974	1.427352	1.431747	1.436169
0.080	1.477584	1.482465	1.487380	1.492337
0.085	1.535043	1.540446	1.545901	1.551420
0.090	1.595298	1.601240	1.607259	1.613367
0.095	1.658300	1.664800	1.671405	1.678129
0.100	1.724007	1.731082	1.738298	1.745669
0.105	1.792382	1.800052	1.807904	1.815954
0.110	1.863393	1.871677	1.880193	1.888956
0.115	1.937012	1.945932	1.955140	1.964653
0.120	2.013216	2.022795	2.032727	2.043030
0.125	2.091985	2.102247	2.112937	2.124075
0.130	2.173303	2.184276	2.195762	2.207781
0.135	2.257157	2.268871	2.281194	2.294146
0.140	2.343539	2.356026	2.369231	2.383174
0.145	2.432439	2.445736	2.459873	2.474869
0.150	2.523855	2.538002	2.553126	2.569244

<sup>A</sup> For cylindrical rods  $K = 1/4$ , and for rectangular bars  $K = 1/3.4641$ .

**TABLE 2 Correction Factor,  $T_2$ , for the First Overtone of Flexural Vibration**

$K (t/L)^A$	Poisson's Ratio			
	0.15	0.20	0.25	0.30
0.0000	1.000000	1.000000	1.000000	1.000000
0.0025	1.001422	1.001445	1.001467	1.001489
0.0050	1.005683	1.005774	1.005863	1.005952
0.0075	1.012770	1.012973	1.013174	1.013373
0.0100	1.022660	1.023019	1.023376	1.023728
0.0125	1.035326	1.035885	1.036440	1.036987
0.0150	1.050734	1.051537	1.052327	1.053108
0.0175	1.068844	1.069926	1.070995	1.072054
0.0200	1.089613	1.091015	1.092401	1.093775
0.0225	1.112996	1.114756	1.116497	1.118223
0.0250	1.138949	1.141103	1.143235	1.145352
0.0275	1.167429	1.170012	1.172573	1.175115
0.0300	1.198394	1.201441	1.204465	1.207470
0.0325	1.231807	1.235353	1.238874	1.242376
0.0350	1.267633	1.271711	1.275764	1.279800
0.0375	1.305844	1.310487	1.315106	1.319710
0.0400	1.346414	1.351656	1.356876	1.362084
0.0425	1.389325	1.395199	1.401055	1.406905
0.0450	1.434563	1.441104	1.447633	1.454162
0.0475	1.482122	1.489364	1.496602	1.503850
0.0500	1.532000	1.539980	1.547966	1.555973
0.0525	1.584202	1.592958	1.601732	1.610540
0.0550	1.638741	1.648312	1.657917	1.667572
0.0575	1.695636	1.706063	1.716543	1.727092
0.0600	1.754912	1.766240	1.777642	1.789136
0.0625	1.816603	1.828880	1.841254	1.853748
0.0650	1.880751	1.894027	1.907428	1.920979
0.0675	1.947405	1.961734	1.976222	1.990892
0.0700	2.016625	2.032066	2.047703	2.063560
0.0725	2.088477	2.105095	2.121950	2.139068
0.0750	2.163041	2.180906	2.199055	2.217513
0.0775	2.240405	2.259595	2.279119	2.299006
0.0800	2.320672	2.341270	2.362262	2.383673
0.0825	2.403955	2.426056	2.448613	2.471654
0.0850	2.493833	2.514090	2.538324	2.563111
0.0875	2.580098	2.605527	2.631559	2.658220
0.0900	2.673262	2.700540	2.728506	2.757184

where:

$$G = \text{shear modulus, kgf/cm}^2,$$

$$B = \frac{4L}{bt} \left[ \frac{b/t + t/b}{4(t/b) - 2.52(t/b)^2 + 0.21(t/b)^6} \right]$$

and

$A$  = correction factor dependent on the width-to-thickness ratio of the test specimen. (See Fig. 6 for a plot of  $A$  as a function of the width to thickness ratio.)

7.2.2 For the fundamental torsion of a cylindrical rod:

$$G = (2Lw_f^2 \times 10^{-3})/\pi r^2 \quad (6)$$

where:

$$G = \text{shear modulus, kgf/cm}^2, \text{ and}$$

$$r = \text{radius of rod, cm.}$$

7.3 Poisson's Ratio:

$$\mu = (E/2G) - 1 \quad (7)$$

<sup>4</sup> Shear modulus correction taken from: Spinner, S., and Valore, R. C., "Comparison of Theoretical and Empirical Relations Between the Shear Modulus and Torsional Resonance Frequencies for Bars and Rectangular Cross Sections," *Journal of Research*, National Bureau Standards, Vol 60, 1958, RP2861, p. 459.

6). Their work was presented in the following journals:

Pickett, G. "Equations for Computing Elastic Constants from Flexural and Torsional Resonant Frequencies of Vibration of Prisms and Cylinders," *Proceedings*, ASTM Vol. 45, 1945, pp. 846-865.

Goens, E. "Über die Bestimmung des Elastizitätsmoduls von Stüben mit Hilfe von Biegungsschwingungen", *Annalen der Physik*, B. Folge, Band 11, 1931, pp. 649-678.

7.1.2 For the first overtone in flexure of a rectangular bar (Note 5):

$$E = 12.703 (L^3/bt^3) T_2 w_f^2 \times 10^{-8} \quad (2)$$

where:

$T_2$  = correction factor for first overtone in flexure. (See Table 2 for a plot of  $T_2$  as a function of bar dimensions and Poisson's ratio.)

7.1.3 For the fundamental in flexure of a rod of circular cross section (Note 5):

$$E = 1.6408 (L^3/D^4) T_1 w_f^2 \times 10^{-6} \quad (3)$$

where:

$D$  = diameter of rod, cm.

7.1.4 For the first overtone in flexure of a rod of circular cross section (Note 5):

$$E = 21.567 (L^3/D^4) T_2 w_f^2 \times 10^{-8} \quad (4)$$

7.2 Shear Modulus:

7.2.1 For the fundamental torsion of a rectangular bar (Note 5):<sup>4</sup>

$$G = (10.197 B w_f^2 \times 10^{-7})/(1 + A) \quad (5)$$

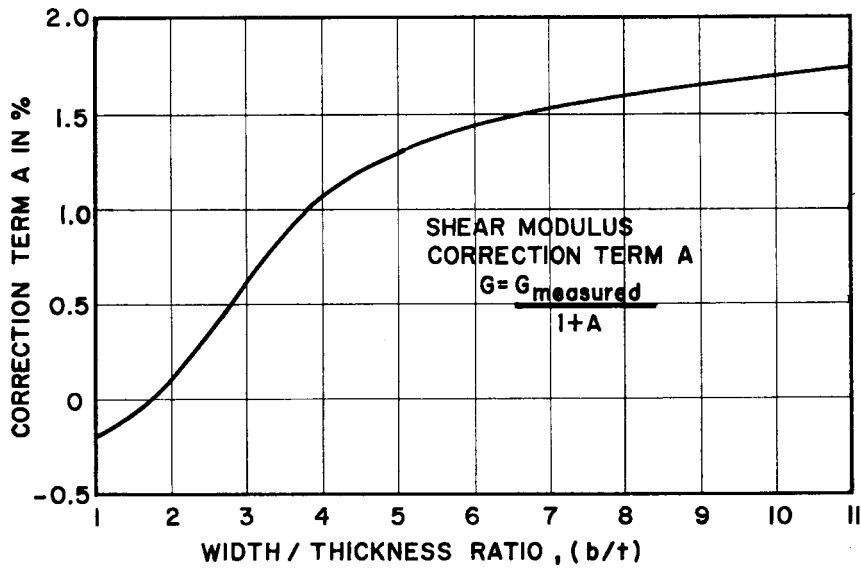


FIG. 6 Plot of the Shear Modulus Correction Term A

where:

- $\mu$  = Poisson's ratio,
- $E$  = Young's modulus, and
- $G$  = shear modulus.

7.4 Calculation of moduli at elevated and cryogenic temperatures:

$$M_T = M_o [f_T/f_o]^2 [1/(1 + \alpha\Delta T)] \quad (8)$$

where:

- $M_T$  = modulus at temperature  $T$ ,
- $M_o$  = modulus at room temperature,
- $f_T$  = resonance frequency in furnace or cryogenic chamber at temperature  $T$ ,
- $f_o$  = resonance frequency at room temperature in furnace or cryogenic chamber,
- $\alpha$  = average linear thermal expansion coefficient of specimen from room temperature to test temperature, cm/cm·°C, and
- $\Delta T$  = temperature differential, test temperature from room temperature.

## 8. Report

8.1 Report the following information:

8.1.1 Identification of specific tests performed and apparatus used,

8.1.2 Complete description of material(s) tested stating its composition, melt number, annealing schedule or ceramming schedule, and any other treatment such as chemical strengthening, etc., to which it has been subjected. Comments on surface finish, edge conditions, etc. shall be included where pertinent,

8.1.3 Name of person requesting test,

8.1.4 Laboratory notebook number and page on which test data is recorded; file number if used, and

8.1.5 Numerical values obtained for Young's modulus, shear modulus, and Poisson's ratio.

## 9. Precision and Bias

9.1 Precision and bias on the order of 1 % for moduli and 10 % for Poisson's ratio is possible if all tolerances on dimensions are observed, resonance frequencies are measured with a frequency counter, and the weight of the specimen is measured within 10 mg.

## 10. Keywords

10.1 glass; Poisson's ratio; resonance; shear modulus; Young's modulus

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